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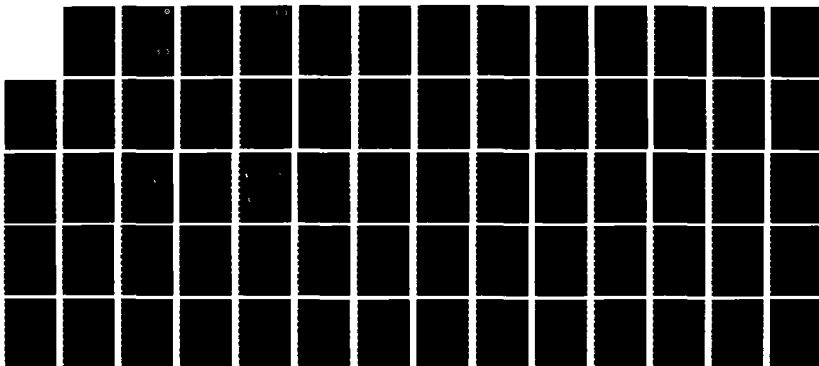
DESIGN AND OPERATION OF THE FORWARD SCATTERING METER  
(U) NAVAL RESEARCH LAB WASHINGTON DC J E JAMES ET AL.  
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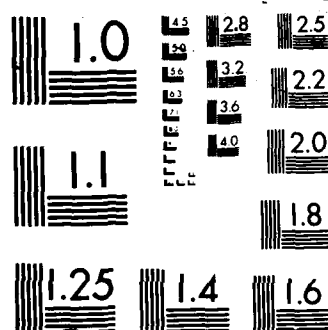
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# Naval Research Laboratory

Washington, DC 20375-5000    NRL Report 8996    October 18, 1986



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## Design and Operation of the Forward Scattering Meter

JEFFREY E. JAMES AND H. GERBER

*Atmospheric Physics Branch  
Space Science Division*

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## CONTENTS

INTRODUCTION .....	1
THEORY OF OPERATION .....	1
DESIGN OF FSM .....	2
Transmitter .....	2
Detector .....	3
Sensor Mount and Enclosure .....	4
Electronics .....	5
General Description .....	5
Amplifier Board and Lock-in Amplifier .....	6
Cables and Connectors .....	9
OPERATION OF FSM .....	12
Deployment .....	12
Front Panel Controls .....	12
Start-Up Procedure .....	14
Manual Operation .....	15
Calibration .....	16
Field Calibration .....	16
Prime Calibration .....	16
Precautions .....	16
FIELD TEST .....	17
RECOMMENDATIONS .....	19
Laser High-Voltage Supply .....	19
Detector Signal Amplifiers .....	19
Sensor Outer Casing .....	19
Cables and Connectors .....	19
Future Development .....	19
ACKNOWLEDGMENTS .....	20
REFERENCES .....	20
APPENDIX A — Specifications .....	21
APPENDIX B — Parts List .....	23
APPENDIX C — Drawings .....	26



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# DESIGN AND OPERATION OF THE FORWARD SCATTERING METER

## INTRODUCTION

The Forward Scattering Meter (FSM) was developed for the Shipboard Meteorological and Oceanographic Observation System (SMOOS) program, in response to an operational requirement to measure the infrared (IR) extinction of maritime aerosol as specified in OPNAVINST 5000.42B [1]. The FSM measures visible laser light (632.8 nm) scattered by airborne particles into the near forward direction. This light is directly proportional to the extinction coefficient of the aerosol in the far infrared, such as at the 10.6  $\mu\text{m}$  wavelength. The FSM is capable of measuring the forward scattered light down to one part per one hundred thousand of the direct laser intensity, which gives it a wide range of sensitivity including infrared estimates in hazes and fogs. The FSM's design reflects the need to protect optical instruments from the harsh environment found aboard ship.

The extinction coefficient is used to determine the performance of infrared systems such as Forward Looking Infrared Radar (FLIR) and to serve as a boundary value for modeling the vertical dependence of atmospheric optics that influence optically guided missiles and other optical devices.

This report is intended to be used as a guideline for the production of the FSM. It considers the theoretical aspects as well as the mechanical and electronics design. A field test was conducted at the Calspan Corp. test chamber in which the FSM was subjected to aerosols of various sizes and concentrations. Data obtained show that this instrument works as designed. Problems found during the construction and field test of the FSM are discussed, and recommendations are given to resolve them.

## THEORY OF OPERATION

Figure 1 gives a simplified schematic of the FSM and demonstrates its principle of operation. A collimated HeNe laser beam is passed through a length  $L$  of ambient aerosol consisting of maritime haze or fog. The beam is aligned to pass into a light trap placed in front of a detector consisting of a photodiode. In this manner the detector does not see the direct light from the laser beam but only the light scattered into the near-forward direction by the aerosols passing through the beam. (Aerosols scatter light in all directions; in the present arrangement only the light scattered over a small range of angles in the direction of beam propagation is intercepted by the photodiode.) The fraction  $F$  consisting of the intensity of the forward-scattered light divided by the intensity of the laser beam is given by the expression [2]:

$$F = \frac{\lambda^2}{4\pi} \int_{r_1}^{r_2} \int_{\theta_1}^{\theta_2} \int_{\gamma_1}^{\gamma_2} (i_1 + i_2) \cos \theta n(r) dr d\theta d\gamma, \quad (1)$$

where  $i_1$  and  $i_2$  are the Mie intensity functions [3],  $\theta$  is the angle between the optical axis and the line between the scattering point in the beam and the location on the detector,  $n(r)$  is the size distribution of the aerosol particles,  $\gamma$  is the radial distance along the active surface of the photodiode, and  $\lambda$  is the wavelength of light.

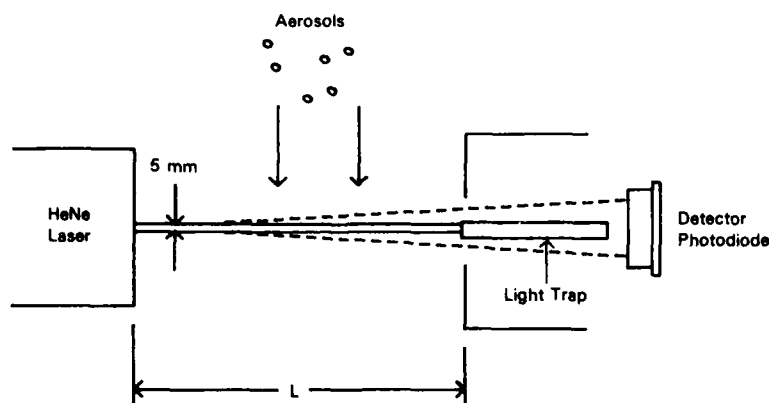


Fig. 1 — Simplified schematic diagram of the operation of the FSM

It was predicted [2,4] that Eq. (1) reduces to an approximately linear relationship between  $F$  and the far-infrared aerosol extinction:

$$F = \frac{\sigma_e (10.6 \mu\text{m})}{A}, \quad (2)$$

where  $\sigma_e (10.6 \mu\text{m})$  is the aerosol extinction coefficient at a wavelength of  $10.6 \mu\text{m}$ ; and  $A$  is a constant that depends on the measured angular range of the forward scattered light, on the specific geometry of the instrument, and on the composition of the aerosol particles. Equation (2) is independent of  $n(r)$  and is valid for aerosol particle sizes found in typical maritime hazes and fogs.

It was estimated [4] that Eq. (2) can predict  $\sigma_e (10.6 \mu\text{m})$  with an accuracy of  $\pm 10\%$  for maritime aerosol, which usually consist of particles with a high water content and thus are of similar composition. It is expected that a relationship similar to Eq. (2) also holds for broad wavelength intervals in the 8 to  $10 \mu\text{m}$  window.

## DESIGN OF FSM

### Transmitter

In designing the transmitter assembly, the optical and the mechanical aspects must be considered. The optics consist of three components (see Fig. 2); a Melles-Griot HeNe laser operating at  $632.8 \text{ nm}$  with an output intensity of  $2 \text{ mW}$ ; a Melles-Griot spatial filter with a focal length of  $12 \text{ mm}$ , maximum aperture of  $4.8 \text{ mm}$ , wavelength range of  $450$  to  $750 \text{ nm}$ , and pinhole assembly with a pinhole diameter of  $40 \mu\text{m}$ ; and a Melles-Griot collimator modified for a focal length of  $51 \text{ cm}$  ( $20 \text{ in.}$ ) and outfitted with a synthetic, fused quartz singlet lens from the Republic Lens Company. Of utmost importance in the design of the transmitter is the use of a high-quality collimator lens. Background noise measured at the detector is directly related to the quality of this lens. Since the Melles-Griot collimator lens lacked the desired quality, it was replaced with the synthetic, fused quartz lens. A special adaptor was needed to accommodate the new lens. See Appendix B for detailed drawings.

The laser beam passes through a cylindrical chopper that has two holes drilled through it at right angles to each other (see drawing in Appendix B). The beam is chopped at  $20 \text{ Hz}$ . The laser beam then passes through the spatial filter and pinhole assembly, which filters out the higher order diffraction patterns from the beam and gives a precise Gaussian power distribution. Adjustment knobs are found on the spatial filter assembly for positioning the pinhole at the exact center of the beam and for focusing the beam onto the plane of the pinhole. The laser beam then passes through the collimator. The collimator focuses the beam to a small point in the light trap that is concentric with the detector. Modifications were made to the collimator to obtain a shorter focal length; see Appendix B.

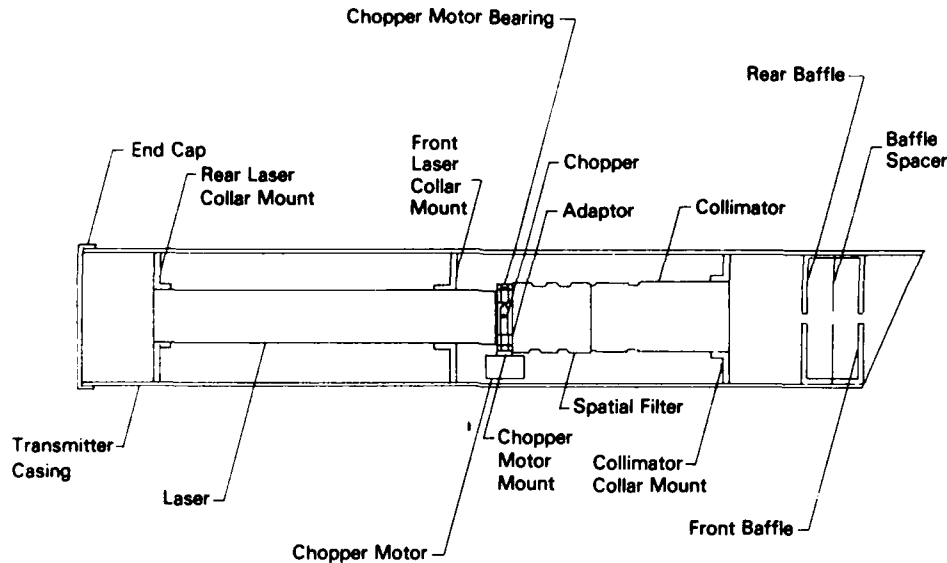


Fig. 2 — Cross-sectional view of the transmitter assembly

Mechanical aspects must also be considered in the design of the transmitter assembly. The laser and related optics are housed in a hinged, cylindrical casing that permits easy access to the focusing rings of the optics. Enough space must exist in the housing to allow access to the pinhole adjustments as well as for freedom of movement of the focusing rings. The optical components are mounted with circular aluminum collar mounts. Holes drilled in the mounts let filtered air pass through to the collimator lens. The chopper motor is mounted on the Melles-Griot adaptor with the chopper motor mount. The adaptor was modified at NRL to allow the chopper to pass through the optical axis. The chopper is mounted to the chopper motor and is inserted in a bearing at the top of the chopper motor mount. A reference photodiode is epoxied to the inside of the adaptor.

The transmitter is weatherproofed for the harsh marine environment. The rear cap has a 3/4 in. lip and a 1/16 in. neoprene gasket to prevent salt water, rain, or other contaminants from entering. The mating edges of the hinged housing are also gasketed. The front of the transmitter utilizes a baffle assembly that keeps out large particles such as rain and salt spray. The baffle consists of two chambers and three walls with 1/2 in. holes bored in each to permit the laser beam to pass through. A filtered air system is employed in the design. An air compressor blows filtered air through the rear of the transmitter and out the front, further protecting the lenses from contaminants.

### Detector

The detector's optics consist of several components: three grade A fused silica laser lenses made by Optics for Research; a 632.8 nm narrowband laser filter made by Oriel Corporation; and an assembly designed for housing the lenses, focusing, and fixing the field of view (see Fig. 3). The field of view is determined by several components in the front detector housing. These components include the light trap, the front baffle, the front lens-baffle, and the field stop. The forward scattered light that falls within the field of view is focused by lens A to a pinpoint in the same plane as the field stop. Lens B in the rear detector housing collimates the scattered light passing through the field stop. This gives the required, near-parallel light that passes through the laser-line filter. The filter gives a low-light background for all wavelengths of light other than the 632.8 nm wavelength of the laser. Lens C focuses the scattered light onto the sensitive area of the detector photodiode. The front and rear detector housings are threaded and are adjusted with respect to one another so that lens B focuses on the field stop. Lockrings are utilized to ensure permanent location of parts once they have been focused. All parts are black anodized aluminum.



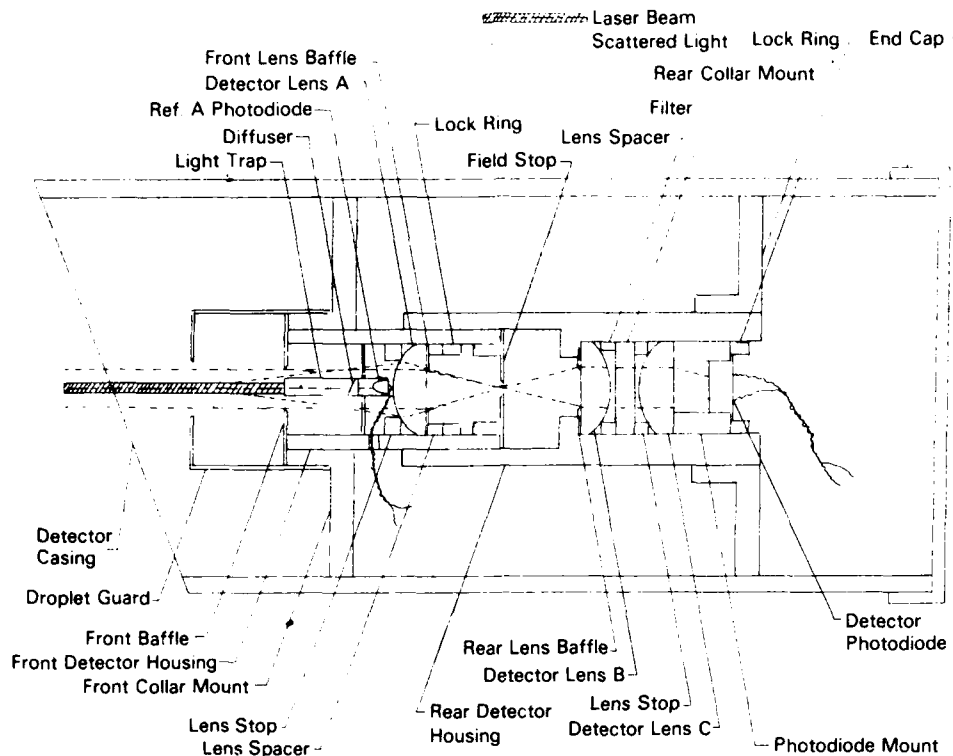


Fig. 3 — Cross-sectional view of the detector assembly

The detector is housed in a cylindrical casing and is mounted with circular aluminum collar mounts. The rear mount has several 1/2 in. holes bored in it to allow filtered air to pass along the casing. The front mount is solid so as to force the filtered air through the holes drilled in the detector front housing, which in turn passes the air over the front lens. The light trap is mounted with 20 gage piano wire. Holes are drilled through the light trap and the front detector housing at right angles to each other. The piano wire is passed through these holes and epoxied at the ends. Weatherproofing of the detector is accomplished much the same as with the transmitter. Filtered air is passed over lens A to keep out small airborne particles. A neoprene gasket is used on the rear cap to prevent salt water and rain from entering, and a droplet guard is used on the front of the detector to keep out large airborne particles. All aluminum parts are black anodized, and parts exposed to the elements are painted with a white, polyurethane base paint.

### Sensor Mount and Enclosure

The transmitter and detector are mounted on a 5 in. wide aluminum H-beam with cradle mounts. See Fig. 4 and drawings in Appendix B. An H-beam was used for the sensor base because of the need for a rigid structure on which to align the transmitter and detector. The open section between the transmitter and detector was removed from the H-beam so there would be no significant surface area on which rain and sea spray could bounce off into the path of the laser beam as this would cause a faulty output. The sensor is mounted to the ship with the sensor mount. The sensor mount has a 1/2 in. rubber shock mount to reduce damage caused by vibration. The sensor mount will accept a standard 1-in. pipe, or the bracket mount can be installed so that the sensor can then be mounted on a horizontal or vertical rail from 1 to 3 in. in diameter. The sensor and mounts are painted with a white, polyurethane base paint to give added protection from the elements.

The electronics enclosure is made by General Metals Corp. and is constructed of 1/8 in. stainless steel. All seams are continuously welded to ensure a waterproof seal. The enclosure's outer door has a

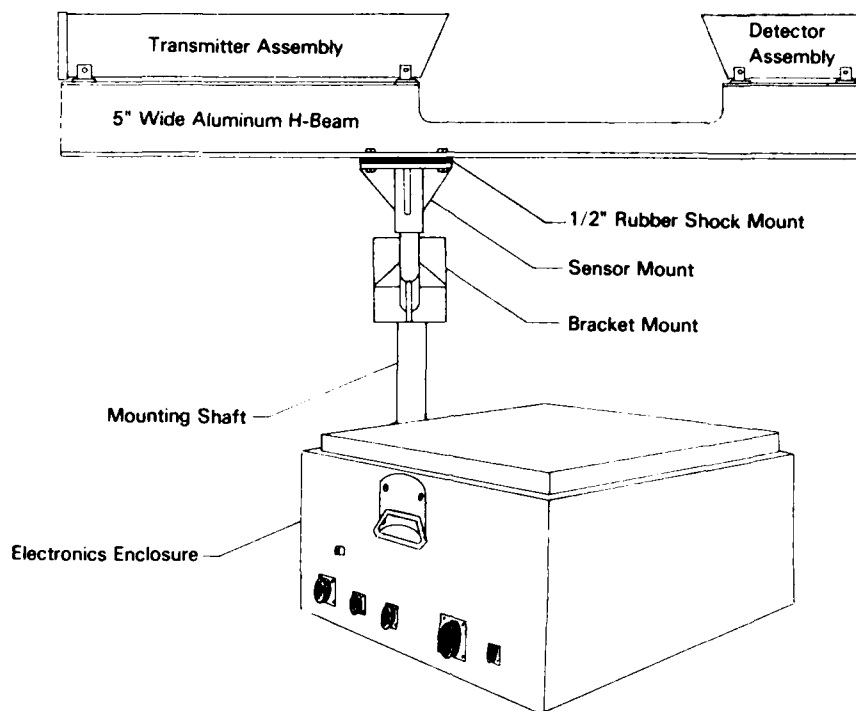


Fig. 4 — The FSM

built-in lip with a 1/8 in. neoprene gasket to keep water out. A continuous hinge on the outer door provides a strong, long-lasting outer door. The inner door is used to mount the power switches, fuses, and display. The electronics enclosure has a row of air filters mounted on one side to provide clean air-flow to the electronics. A fan is mounted on the opposite side of the enclosure to circulate air and to help remove heat created by the air compressor and laser power supply. The enclosure is also painted with the white polyurethane base paint.

## Electronics

### *General Description*

The electronics of the FSM consists of two TIL78 Phototransistors, an RCA C30809 Photodiode, an amplifier circuit utilizing LM307's, an Evans Electronics Lock-in amplifier, and a Kiethly 195T Programmable Digital Multimeter. See Fig. 5 for a simplified schematic.

The detector signal is obtained by reverse biasing the RCA C30809 detector photodiode with 45 Vdc. This signal is then amplified and fed to switch 3. Switch 3 is a two-position switch whose common terminal is connected to the signal input of the lock-in amplifier. This switch is used to check for zero output of the FSM when the detector signal is grounded.

Two reference signals are used in the design. The light trap reference is obtained by reverse biasing the TIL78 located in the light trap with 30 Vdc and serves as the lock-in amplifier reference signal. This reference is then amplified and fed to switch 4. Switch 4 is utilized in the calibration of the FSM. It switches between the reference signal and the detector signal when the calibration assembly is attached. The common terminal of switch 4 is connected to the reference input of the lock-in amplifier.

The adaptor reference is obtained by reverse biasing the TIL78 located in the Melles-Griot adaptor with 30 Vdc and serves as a laser intensity reference. This reference is then amplified, converted to

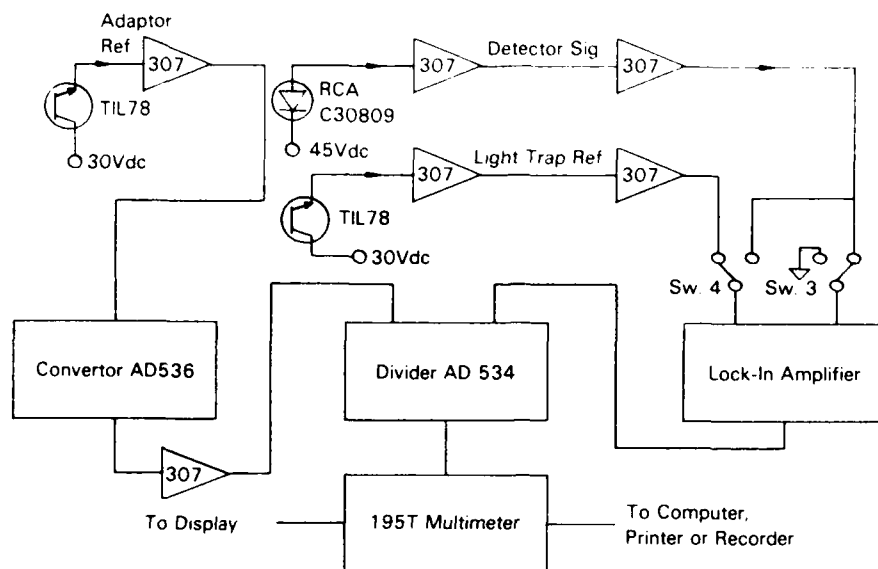


Fig. 5 — Simplified flow chart shows the paths of the light trap reference, the adaptor reference, and the detector signal

a dc voltage that corresponds to its RMS value, and amplified to the desired level. There were two reasons why two reference signals were used. First, any misalignment between the laser and the light trap due to the warping of the H-beam could significantly change the amplitude of the light-trap reference signal, therefore making questionable the use of the light-trap reference as a laser intensity reference. Second, the lock-in amplifier reference input must be in phase with the lock-in signal input. The adaptor reference is obtained by using light reflected off the chopper causing it to be distorted and partially out of phase with the detector signal, therefore making it undesirable as a lock-in reference input. The adaptor reference and the detector signal are then fed into the AD536 divider on the amplifier board. The divider ratios between the detector signal and the adaptor reference signal to rid the output of laser intensity fluctuations. The output of the divider is then sent to the digital multimeter for A/D conversion and output to the recording instrumentation.

### Amplifier Board and Lock-in Amplifier

The amplifier board consists of three signal amplifier circuits, a voltage regulator circuit, an AD534 divider, and an AD536 RMS to dc converter. Refer to Fig. 6 and Tables 1, 2, and 3 for the following description. The voltage regulator circuit uses an LM350K voltage regulator. The input to the regulator (pin 8 on the edge connector) is 45 Vdc. The output of the voltage regulator (pin 10 on the edge connector) should be set to 30 Vdc and is adjustable through potentiometer P1. This voltage is used for reverse biasing the TIL78 phototransistors.

The detector signal is fed into a two-stage inverting operational amplifier circuit (pin 12 on the edge connector) via shielded cable. Gain is adjustable through potentiometer P4. The output of the amplifier circuit (pin 16 on the edge connector) is then fed into the ac signal input (pin 18) of the Evans Electronics lock-in amplifier. The lock-in amplifier gives a dc voltage corresponding to the RMS value of the incoming signal. The lock-in amplifier reduces noise on the signal by only amplifying the signal in phase with the light-trap reference signal. The output of the lock-in amplifier (pin 10) is then fed into the AD534 divider IC (pin 14 on the edge connector) on the amplifier board.

The light-trap reference signal is fed into a two-stage inverting operational amplifier circuit via pin 3 of the amplifier board. It is then fed into the ac reference input (pin 3) of the lock-in amplifier. Gain is adjustable through potentiometer P3.

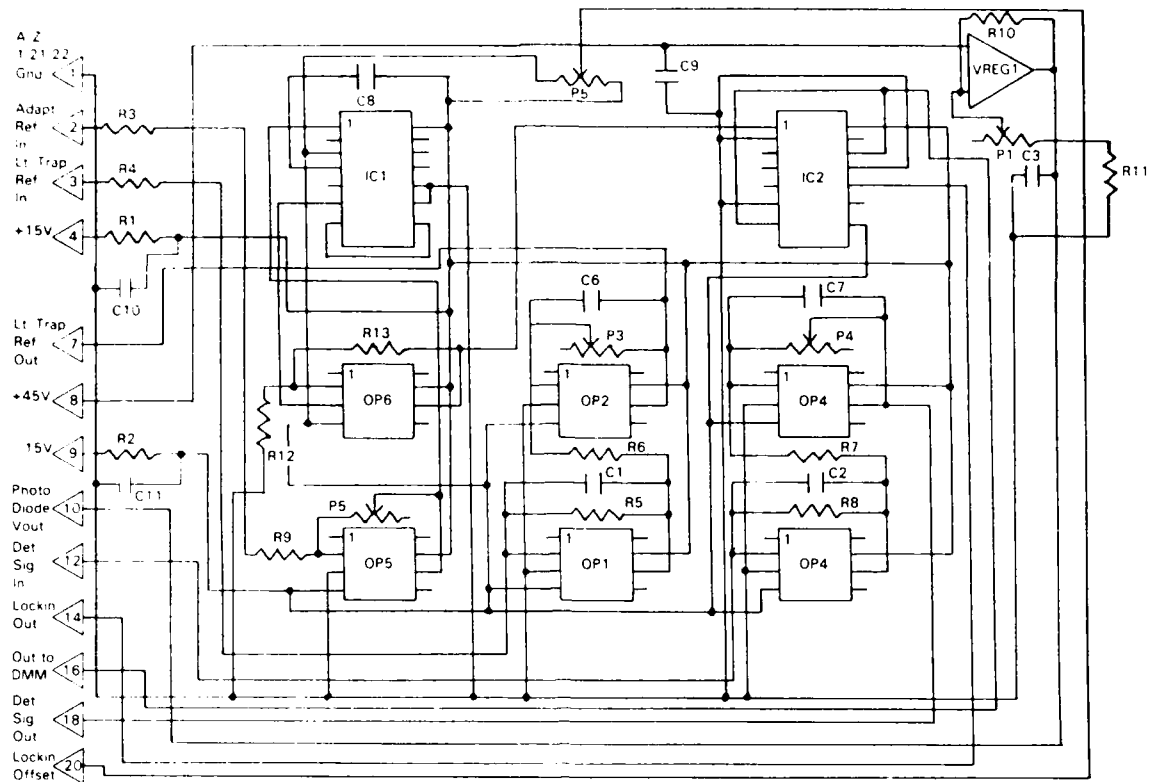


Fig 6 — Schematic diagram of the FSM amplifier board

Table 1 — Amplifier Board Parts Identification

Item	Quantity	Part Desc.	Part #	Board Loc.
1.	2	Resistor	100	R1, R2
2.	6	Op. Amp.	LM307	OP1-OP6
3.	1	Volt Reg.	LM350K	VREG 1
4.	3	Resistor	1K	R3-R5
5.	2	Resistor	5K	R6, R7
6.	1	Resistor	200K	R8
7.	1	Resistor	1K	R9
8.	1	Pot.	2K	P1
9.	1	Pot.	5K	P2
10.	2	Pot.	50K	P3, P4
11.	1	Pot.	20K	P5
12.	1	Edge Conn.	22 pin	CON1
13.	1	Ckt. Board	Vector	B1
14.	5	I.C. Socket	8 pin	S1-S5
15.	2	I.C. Socket	14 pin	S6-S7
16.	2	Capacitor	1.5 $\mu$ F 50V	C1, C2
17.	1	Capacitor	1 $\mu$ F 50V	C3
18.	2	Capacitor	.1 $\mu$ F	C4, C5
19.	1	RMS/DC	AD534	IC1
20.	1	Divider	AD536	IC2
21.	2	Resistor	120	R10, R11
22.	1	Resistor	2K	R12
23.	1	Resistor	51K	R13
24.	2	Capacitor	.047 $\mu$ F	C6, C7
25.	1	Capacitor	100 $\mu$ F	C8
26.	1	Capacitor	.1 $\mu$ F	C9

Table 2 — Amplifier Board Edge Connections

<u>Component Side</u>			<u>Soldered Side</u>
Ground	1	A	Ground
Reference Signal In (Adapter)	2	B	Ground
Reference Signal In (Light Trap)	3	C	Ground
+15Vdc	4	D	Ground
No Connection	5	E	Ground
No connection	6	F	Ground
Reference Signal Out (Light Trap)	7	H	Ground
+ 45Vdc	8	J	Ground
- 15Vdc	9	K	Ground
Voltage Out (For Photodiodes)	10	L	Ground
No Connection	11	M	Ground
Detector Signal In	12	N	Ground
No Connection	13	P	Ground
Output From Lock-In	14	R	Ground
No Connection	15	S	Ground
Output To Multimeter	16	T	Ground
No Connection	17	U	Ground
Signal Out (To Lock-In)	18	V	Ground
No Connection	19	W	Ground
Offset (Lock-In)	20	X	Ground
No Connection	21	Y	Ground
Ground	22	Z	Ground

Table 3 — Lock-in Amplifier Edge Connections

<u>Soldered Side</u>			<u>Component Side</u>
Ground	22	Z	Ground
AC Signal Input	21	Y	Ground
DC Signal Input	20	X	Ground
Ground	19	W	Ground
No Connection	18	V	Ground
Offset	17	U	Ground
20 DB	16	T	Ground
40 DB	15	S	Ground
Filter	14	R	Ground
DC	13	P	Ground
20 DB Post	12	N	Ground
Overload	11	M	Ground
Output	10	L	Ground
Signal Monitor	9	K	Ground
CB	8	J	Ground
CA	7	H	Ground
-15 V	6	F	-15 V
+15 V	5	E	+15 V
Logic Reference Input	4	D	Ground
AC Reference Input	3	C	Ground
DC Reference Input	2	B	Level Shift
Ground	1	A	Ground

The adaptor reference signal is fed into a single-stage inverting operational amplifier circuit via pin 2 of the amplifier board with gain adjustable through potentiometer P2. It is then fed into the input of the AD536 RMS to dc converter. The AD536 gives a dc voltage corresponding to the RMS value of the incoming signal. The output of the RMS to dc converter is fed into a noninverting operational amplifier for amplification to the desired voltage level of approximately 8 V. The adaptor reference signal is then fed into the AD534 divider. This divider ratios between the output of the RMS to dc converter and the output of the Evans Electronics Lock-In amplifier, reducing detector signal errors caused by laser intensity fluctuation errors.

Output of the AD534 Divider IC:

$$\text{Output} = 10 * \frac{(X1 - X2)}{(Z2 - Z1)} + Y1 \quad (3)$$

where

- 10 = Gain of AD534 Divider IC
- X1 = Detector signal
- X2 = Ground (0)
- Z2 = Adaptor reference signal
- Z1 = Ground (0)
- Y1 = Ground (0)

The output of the AD534 divider is then fed into the input of the Keithly 195T Programmable Digital Multimeter. The 195T is programmed to fill a 100-point buffer and do a running average of the data stored. This average is then sent over the IEEE-488 bus when signaled to do so.

#### *Cables and Connectors*

The FSM uses shielded cable to reduce noise pickup and interference. The detector cable and adaptor reference/chopper cable use a 6-conductor, 18-gage, individually shielded pair Belden cable (part number 9773). The shield used in this cable is of the continuous foil type and gives 100% coverage. The power cable to the Melles-Griot laser is Belden RG213 coaxial cable rated at 5000 V. The GPIB cable used is a standard 24 conductor, shielded, IEEE 488 interface cable at a modified length of 30 ft. The AC power line is a standard 18 gage, three-conductor cable. For cable connection diagram refer to Fig. 7.

All connectors used in the FSM are Bendix weatherproof connectors. The following pages identify the functions of the connector pins. For part numbers see the parts list in Appendix B of this report; also see the Recommendations section of this report.

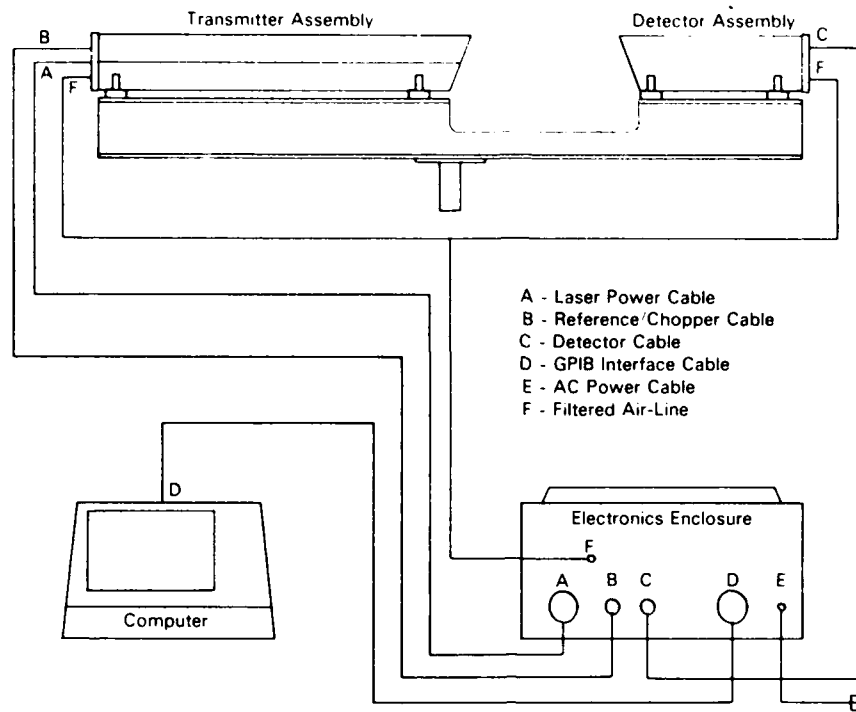


Fig. 7 - Cable connections of the FSM

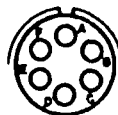
### Detector Signal Cable

Bendix Conn. Pin	Signal Type
A	Light trap reference signal
B	Detector signal
C	Shield (detector signal)
D	+45 Vdc (detector bias)
E	Shield (light trap reference signal)
F	+30 Vdc (light trap reference bias)



### Reference/Chopper Cable

Bendix Conn. Pin	Signal Type
A	110 Vac hot (chopper motor)
B	Shield (adapter reference)
C	Adapter reference signal
D	30 Vdc (adapter reference)
E	AC ground (chopper motor)
F	110 Vac neutral (chopper motor)

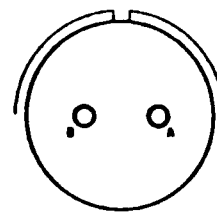


**AC Power Cable**

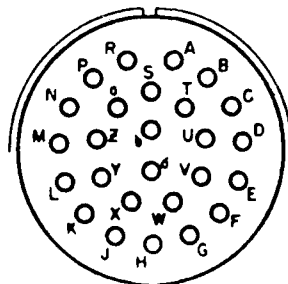
Bendix Conn. Pin	Signal Type
A	AC ground
B	110 Vac (hot)
C	110 Vac (neutral)

**Laser Power Cable**

Bendix Conn. Pin	Signal Type
A	2000 Vdc
B	Ground

**FSM GPIB Computer Interface Cable**

Contact Number	IEEE-488 Designation	Type	Wire Color	Bendix Connection
1	DI01	Data	Brown	A
2	DI02	Data	Red	B
3	DI03	Data	Orange	C
4	DI04	Data	Yellow	D
5	EOI	Management	Green	E
6	DAV	Handshake	Blue	F
7	NRFD	Handshake	Purple	G
8	NDAC	Handshake	Gray	H
9	IFC	Management	White	J
10	SRQ	Management	W/Black	K
11	ATN	Management	W/Brown	L
12	SHIELD	Ground	Uncoated	M
13	DI05	Data	W/Orange	N
14	DI06	Data	W/Yellow	P
15	DI07	Data	W/Green	R
16	DI08	Data	W/Blue	S
17	REN	Management	W/Violet	T
18	Gnd	Ground	W/Grey	u
19	Gnd	Ground	W/Bla/Bro	v
20	Gnd	Ground	W/Bla/Red	w
21	Gnd	Ground	W/Bla/Ora	x
22	Gnd	Ground	W/Bla/Yel	y
23	Gnd	Ground	W/Bla/Gre	z
24	Gnd	Ground	W/Bla/Blue	a
	SHIELD	Shield	Uncoated	b





## OPERATION OF FSM

### Deployment

The FSM consists of:

- |                                  |   |
|----------------------------------|---|
| 1. Sensor                        | 7. 20-ft. laser power cable             |
| 2. Neoprene shock mount          | 8. 20-ft. signal cable                  |
| 3. 1-in. female sensor mount     | 9. 20-ft. reference/chopper power cable |
| 4. Vertical/horizontal bar mount | 10. 30-ft. ac power cable               |
| 5. Electronics enclosure         | 11. 30-ft. GPIB cable                   |
| 6. 20-ft. T connection air line  | 12. Calibration assembly                |

The FSM was designed to be mounted aboard ship and is weatherproofed for the harsh marine environment. It should be mounted high enough off the deck of the ship so as to reduce the chance of being doused with green water. A 1-in. female mount and a 3-in. bracket mount are provided for ease of mounting. Cables should be attached as in Fig. 7 with 90° connectors at the sensor end. The ac power cable should be attached last so as not to create a shock hazard. Cables should be taped to the mounting shaft to relieve cable tension on connectors.

A good coat of automobile wax on the outside of the sensor and electronics enclosure as well as silicone grease applied to all bolts will ensure a longer lasting instrument. The electronics enclosure is weatherproofed as is the sensor. It was designed to be welded or bolted to the deck of the ship with 3/8 in. × 16 studs welded on the deck corresponding to the mounting holes of the electronics enclosure.

### Front Panel Controls

The front panel controls are located on the front panel under the electronic enclosures outer door. Access to these controls is obtained by loosening the seven outer door hold-down bolts. Ensure that you are well familiarized with all front panel controls before operating the FSM. The following describes the front panel controls and their functions, see Fig. 8.

1. Power on/off (SW 1)—This switch turns on main power to FSM subassemblies.
2. Laser Power on/off (SW 2)—This keyed switch turns the HeNe laser on or off regardless of main power switch being on.
3. Signal/Ground (SW 3)—This switch is used for zeroing any noise in the amplifier circuit by grounding the signal input. For more information see the Calibration section.
4. Reference/Signal (SW 4)—This switch is used during calibration. It switches between the reference signal and the detector signal for use as the reference. For more information see the Calibration section.
5. Power On Indicator (L 1)—This indicator is lit when power switch (SW 1) is in the on position.
6. Laser On Indicator (L 2)—This indicator is lit when switches (SW 1) and (SW 2) are in the on position.
7. Fuse A (F 1)—This 5A, 250 Vac fuse is for Gast air pump.
8. Fuse B (F 2)—This 3A, Vac fuse is for electronics.
9. Display (D 1)—Six 5 in. LED displays give address, bus information, and data readout. For more information read the Keithley manual.

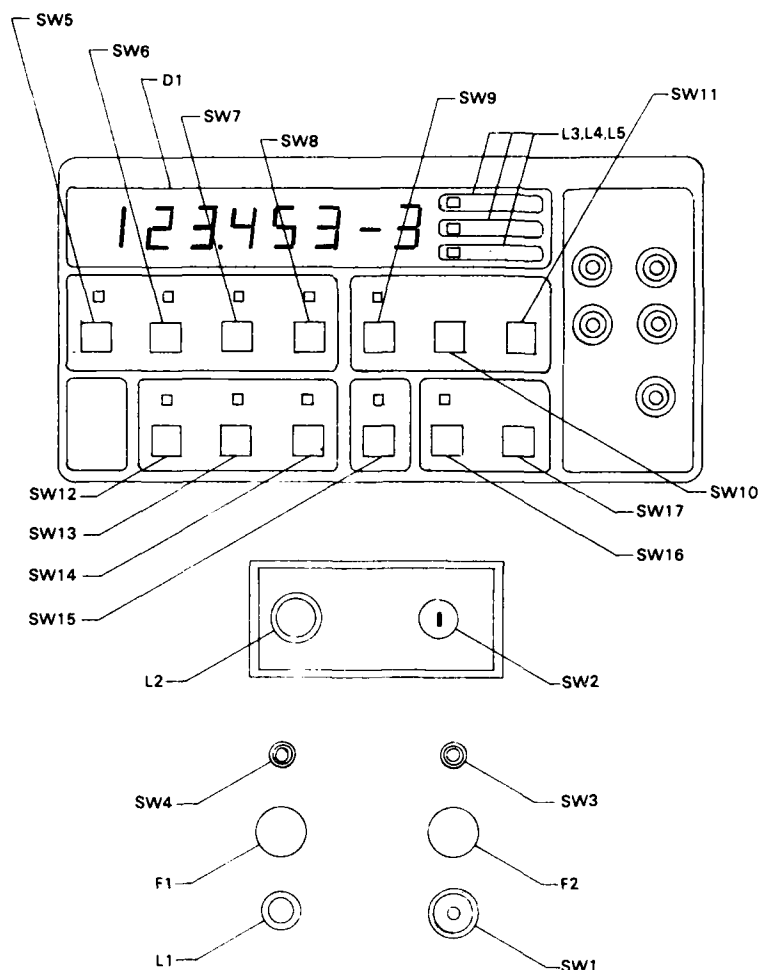


Fig. 8 — Front panel controls

10. Function (SW 5-8)—The four function push buttons control the type of measurement being made.

Volts (SW 5)—For proper FSM operation this push button must be depressed.

Ohms-Amps-AC (SW 6-8)—These push buttons are not used during FSM operation. For more information on these push buttons, see the Keithley 195T Operators Manual.

11. Range (SW 9-11)—The range buttons select the operating ranges of the instrument.

Auto (SW 9)—The auto push button places the 195T in the autoranging mode. This push button should be depressed for FSM operation.

Down-Up (SW 10-11)—These push buttons are not used during FSM operation. For more information on these buttons see the Keithley 195T Operators Manual.

12. Modifiers (SW 12-14)—The modifier buttons control the zero, filter, and resolution modes.

Zero (SW 12)—The zero button controls a zero offset for baseline suppression. Not used during FSM operation.

Filter (SW 13)—The filter button controls the line frequency filter.

Resolution (SW 14)—The resolution button controls the display resolution and should be set for maximum resolution.

13. Trig (SW 15)—This button is not used during FSM operation. See the Keithley 195T Operators Manual for more information.
14. Program (SW 16-17)—The program buttons are used with the front panel programs. The Buffer program is described in Section 5.3. For information on other programs see the Keithley 195T manual.

PRGM (SW 16)—The PRGM button is used as the first step in entering front panel programs 0 to 9.

Recall/Ent (SW 17)—The Recall/Ent button is used to enter and recall data associated with the front panel programs. See the Keithley 195T manual.

15. Terminal Inputs (T1-T5)—The Terminal Inputs are disconnected. The signal is connected via the rear input terminals.
16. IEEE Status (L3-L5) The Remote, Talk, and Listen indicators are used during remote IEEE bus programming. See the Keithley 195T manual for more information.

#### Start-Up Procedure

1. Ensure that the Reference/Signal switch (SW 4) is in the reference position.
2. Ensure that the Signal/Ground switch (SW 3) is in the signal position.
3. Ensure that the laser power cable is connected before turning the laser power supply on, otherwise dangerous arcing may occur.
4. Turn the Laser Power switch (SW 2) to the on position.
5. Turn the Main Power switch (SW 1) to the on position. Note that the red power indicator (L1), laser power supply indicator (L2), and the display panel (D1) illuminate.
6. The display panel (D1) will illuminate with F60A0. The F60 corresponds to the line frequency to which the FSM is set. The A0 is the software revision level of the 195T. In a few seconds it will display the IEEE-488 address, then the 195T will start taking and displaying data.
7. If you are running the FSM by means of a computer capable of operating the GPIB bus, then the following line of code must be sent over the bus.

"FOROS6Q21X"

The F0 sets the 195T to the dc volts scale, and R0 puts the 195T in the autoranging mode. S6 sets the read rate of the 195T. See the rate table in the Keithly 195T manual. Q21 sets the internal buffer to recycle mode for continuously updated data. X tells the 195T that that is the end of command input and to start operating in the selected mode. When an average of the internal buffer is desired, the computer must address the 195T to listen and then send the following line of code.

"U2X"

When this line of code is received by the 195T, it will take the average of the 100-point buffer and send it over the GPIB bus. Your computer must be set up to read this string in and store it. For continuous data acquisition you need not repeat the first line of code, but the second line must be repeated each time an average is desired.

## Manual Operation

If operation of the FSM is to be by the front panel controls, then follow these steps.

1. Depress the volts button (SW 5) once to ensure that the FSM is in the dc volts mode.
2. Depress the autoranging button (SW 9) once to ensure that the autoranging mode is selected.
3. Depress the program button (SW 16). The display (D1) will respond with:  
Pro ?  
Depress the key numbered 7 (SW 13) to specify the data logger program.
4. Depress the Recall/Ent button (SW 17) once. The 195T will display  $r = ?$ . Using the keys numbered 0 to 9 enter the read rate desired.

See the following table for read-rate information. Also see the Keithley manual.

<u>r Value</u>	<u>Read Rate</u>
0	Conversion Rate
1	Same as $r = 0$
2	1-s interval
3	5-s interval
4	10-s interval
5	1-min interval
6	5-min interval
7	10-min interval
8	30-min interval
9	1 h interval

Once you have entered the read rate, you must depress the enter key once again to start the program. The FSM is now in operation. Once the data logger program has filled the 100-point buffer, the display will show BFULL intermittently along with data being taken. At this point you can look at each individual buffer location or get the highest, average, or lowest reading of the buffer.

5. Press the Recall/Ent button (SW 17). The 195T display (D1) will respond with 1 to 100 of the last stored buffer reading as follows:

$$n = (1 \text{ to } 100)$$

6. To read each buffer location continue to press the Recall/Ent button (SW 17); holding the Recall/Ent button down will scroll through the readings rapidly.
7. To obtain an average of the buffer readings, depress the key numbered 3 (SW 9). The instrument will respond with bA. Following this message, the average will be displayed.
8. To obtain the lowest buffer reading press the key numbered 2 (SW 8). The message bL0 will be displayed. Following this message, the lowest buffer reading will be displayed.
9. To obtain the highest reading in the buffer, press the key numbered 1 (SW 7). The message bHI will be displayed. After this message, the highest buffer reading will be displayed. Return to step 1 to restart the data logging process.
10. If any problems are encountered, see the Keithley 195T operators manual.

## Calibration

### Field Calibration

1. Slide the FSM calibration assembly onto the front of the droplet.
2. Power up the FSM. Read the Operation Section for the power-up procedure.
3. Allow a few minutes warm-up time.

Set the Reference/Signal switch (SW 4) to the Signal position. The output of the FSM should be reading within 0.1 V of 2.5 V. If not see the Prime Calibration section.

### Prime Calibration

1. Using a digital voltmeter set to dc volts scale, measure the output (pin 10) of the voltage regulator (VREG1) located on the amplifier board. The output should be set to 30 Vdc and is adjustable through potentiometer P1 (see Fig. 6).
2. Set the Signal/Ground switch (SW 3) to the ground position and the Reference/Signal switch (SW 4) to the reference position (see Fig. 8). The output of the 195T Digital Multimeter should read 0.000 Vdc. If this is not the case, the offset should be zeroed out through potentiometer P5 located on the amplifier board (see Fig. 6).
3. Return the Signal/Ground switch (SW 3) to the Signal position and place the Reference/Signal switch (SW 4) in the Signal position. The output of the 195T Digital Multimeter should read 2.5 Vdc. If it does not, then:
  - a) Use a digital voltmeter set to the dc volts scale, and check for 8 Vdc at the output of OPAMP6 on the amplifier board. If the output is not 8 Vdc, then set it by use of potentiometer P3 on the amplifier board (see Fig. 6).
  - b) Use a digital voltmeter set to the dc volts scale, and check for 2 Vdc at the output of the Evans Electronics Lock-In Amplifier (Pin 10). If not set to 2 Vdc, then adjust through potentiometer P2 on the amplifier board (see Fig. 6). The output of the FSM should read 2.5 Vdc.
  - c) Power down the FSM. Set the Reference/Signal switch (SW 4) to the Reference position. Remove the FSM calibration assembly. The FSM is now calibrated and ready for operation.
4. If this procedure fails to give a correct output, then the lenses may be contaminated or the electronics could be faulty.

### Precautions

1. Do not look directly into the path of the Melles-Griot HeNe laser. Direct eye contact with laser light can cause permanent eye damage.
2. Laser operating voltages may exceed 5000 Vdc, and care should be taken when working near the laser power lines.
3. Line voltages are present in the sensor and the electronics enclosure. Caution should be taken in these areas.
4. Care should be taken not to touch or to contaminate lens surfaces in the transmitter and detector. Clean lenses are a must for accurate operation.

5. Ensure that all cable connections are made before connecting the ac power cable.
6. Be sure that the laser power cable is connected at both ends before turning the laser power supply on. If not, dangerous arcing may occur.
7. The Gast Air Pump will automatically shut off when overheated; it will automatically reset and resume running when cooled to a safe operating temperature.

## FIELD TEST

To validate the predicted performance of the FSM, and to test the practicality of the present FSM design, the output of the instrument was tested against other similar optical measurements in an environmental chamber. A 600-m<sup>3</sup> chamber, located at Arvin/Calspan Corp., was filled with aerosols with a wide variety of size distributions and concentrations, and with a composition similar to what is expected in fogs and hazes of the maritime atmosphere. Simultaneous optical measurements in the chamber consisted of the estimated extinction coefficient at 10.6  $\mu\text{m}$  measured with the FSM, and the photopic extinction coefficient ( $\lambda = 0.55\mu\text{m}$ ) and the extinction coefficient at 10.6  $\mu\text{m}$  measured with Arvin/Calspan transmissometers.

The results of the visible-light and infrared transmissometers are compared in Fig. 9. The data points denoted by circles correspond to cases in which a fog was produced in the chamber by withdrawing air from the chamber during near-saturated conditions. The types of the fog ranged between fogs with few but very large droplets to fogs with many but smaller droplets, also some fogs consisted of a mixture of fog droplets and a large number of haze particles. The data points denoted by x are for cases in which the chamber only contained haze. Various concentration ratios of Salty-Dog pyrotechnic salt particles and nebulizer salt-solution droplets were used to obtain haze-particle size distributions that peaked between about 0.5 to 5  $\mu\text{m}$ . Figure 9 demonstrates, as expected, that aerosol extinction in the visible spectrum is poorly correlated to aerosol extinction in the far infrared, and that no useful scaling relationship between those wavelength regions can be applied.

Figure 10 compares the infrared extinction coefficient at 10.6  $\mu\text{m}$  to the output of the FSM (which measures a fraction of the visible light scattered in the forward direction). The data points have the same interpretation as in Fig. 9. A good correlation exists between the quantities in Fig. 10, and the predicted relationship given by Eq. (2) is essentially verified. The variance of the log of the data points in the direction of the ordinate is  $6.02 \times 10^{-3}$ , which is larger than predicted by theory. The difference can be explained by the variability of the infrared transmissometer measurements owing to systematic instrumentation error, and by the variability of measurements of both instruments owing to the inhomogeneity of the hazes and fogs in the chamber. When the variance caused by these effects is estimated and subtracted from the measured value, the remaining variance approaches the theoretical value that predicts an uncertainty of  $\pm 10\%$  (confidence level of 90%) in the value of the estimated extinction coefficient at 10.6  $\mu\text{m}$  for maritime-type aerosols.

Red phosphorous smoke was used in one of the chamber trials. Again a linear relationship was indicated between the FSM and the infrared transmissometer data; however, in this case the proportionality constant, A, used to scale the FSM reading, was different as expected.

The FSM was run nearly continuously in the chamber for the 1-week period of the trials, with actual exposure to dense aerosols lasting about 15 h. During this period there was no noticeable deterioration in its performance. A major reason for this success was due to the optics of the FSM remaining unaffected by the harsh environment in the chamber. This was accomplished by the FSM's special feature that flushes filtered air past the optics. The precision limit of the FSM measurements, demonstrated in these tests, is given by the observed variation of the instrument's background signal. This variation was about 10 mV at the output of the divider (see the Electronics section of this report), which corresponds to a fraction, F, of forward scattered light of  $\pm 5 \times 10^{-6}$  and an infrared extinction coefficient at 10.6  $\mu\text{m}$  of  $\pm 7 \times 10^{-5}$  1/m.

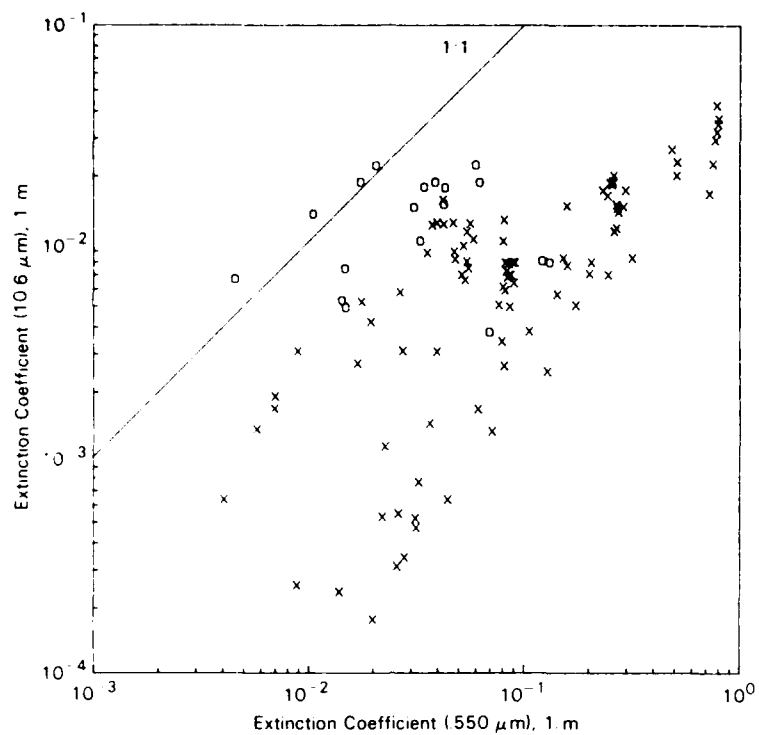


Fig. 9 — Correlation between extinction coefficients measured at  $10.6 \mu\text{m}$  in the infrared and in the visible spectrum. Measurements in the Arvin/Calspan environmental chamber corresponding to fogs are given by circles (○), and those for hazes are given by crosses (×).

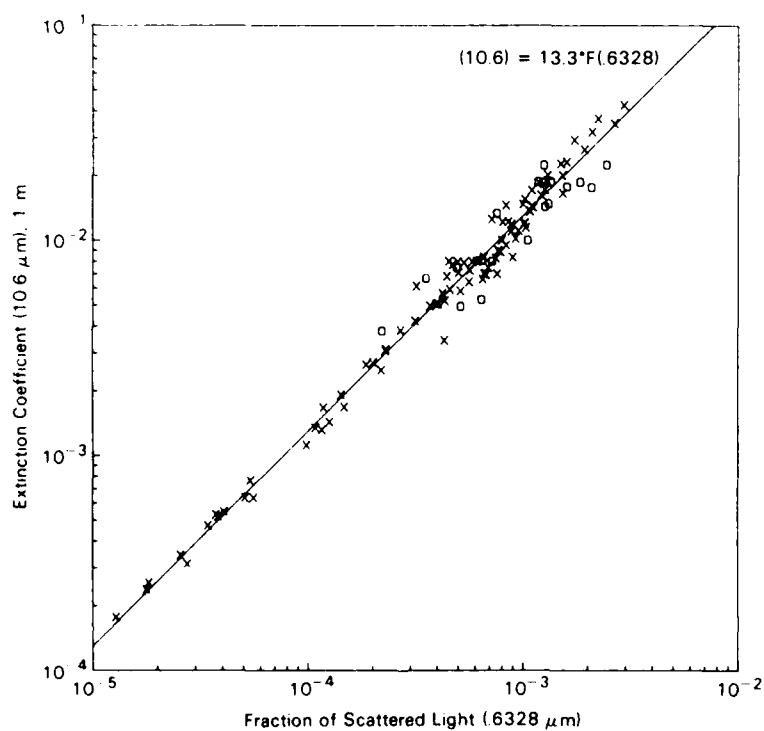


Fig. 10 — Correlation between the aerosol extinction coefficient at  $10.6 \mu\text{m}$  in the infrared and the fraction of visible forward-scattered light measured with the FSM. Data points mean the same as in Fig. 9. The equation gives the geometrical least squares fit of a linear relationship to the data points.

Several improvements in the design of the FSM were suggested by its performance during this field trip; these are given in the next section.

## **RECOMMENDATIONS**

### **Laser High-Voltage Supply**

During the field test at the Calspan chamber, problems arose with the high-voltage supply. Relative humidities of 100% and above were present in the test chamber, which caused condensation to form on the inside of the high-voltage connector at the sensor end. This in turn short circuited the high-voltage supply thus disabling the FSM Meter until the connector could be dried out. It is recommended that a dc to dc upconverter be used in place of the ac-powered high-voltage supply. The upconverter could be mounted near the laser on the H-beam thus eliminating the need for an exposed connector carrying high voltage. A dc to dc upconverter would also reduce the high-frequency noise associated with the ac power supply.

### **Detector Signal Amplifiers**

During the initial testing of the FSM it was found that the detector circuit picked up a significant amount of 60 Hz noise and some distortion caused by the length of the signal cable (20 ft) and the low voltage level of the signal. This noise, when amplified by the detector signal amplifying circuit, causes background noise at the output, reducing the amount of discernible signal. It is therefore recommended that the signal amplifiers be moved as close as possible to the detector photodiode. The amplifiers could be mounted directly on the H-beam. This would significantly reduce the amount of 60 Hz noise. Further reduction would result by using a chopper motor that gives a chopping rate other than an even fraction of 60Hz.

### **Sensor Outer Casing**

During the initial testing of the FSM it was found that the cylindrical housings used for both the detector and the laser made it difficult to gain access to several areas where easy access is necessary. Such areas are the laser and detector components that must be focused. With the present design, the FSM must be partially dismantled to gain access to these controls. It is recommended that a shroud be used in place of the cylindrical housings, and that the laser, its optics, and the detector assembly be mounted directly onto the H-beam with no contact with the shroud or its supports (see Fig. 11). In this design one would only need to remove several screws to remove the shroud and would then have full access to all adjustments.

### **Cables and Connectors**

It was found during use of the FSM that using a single, sensor cable would be beneficial for several reasons. First, a single cable would reduce the number of exposed connectors, which in turn reduces the chance of downtime due to corroded connectors and cables. Second, setup time would be reduced by limiting the number of cables. Also, the chances of outside noise interference would also be reduced. A dc chopper motor could be used, so no ac line voltage need be present on the single cable.

### **Future Development**

The present FSM and the results of the initial field test in the environmental chamber indicate that this approach shows significant promise in resulting in a rugged, reliable, small-sized, and moderately priced device to estimate aerosol far-infrared extinction on Navy ships. Field testing of the FSM in a maritime environment should be undertaken, and a future version of the FSM should implement the preceding recommendations.



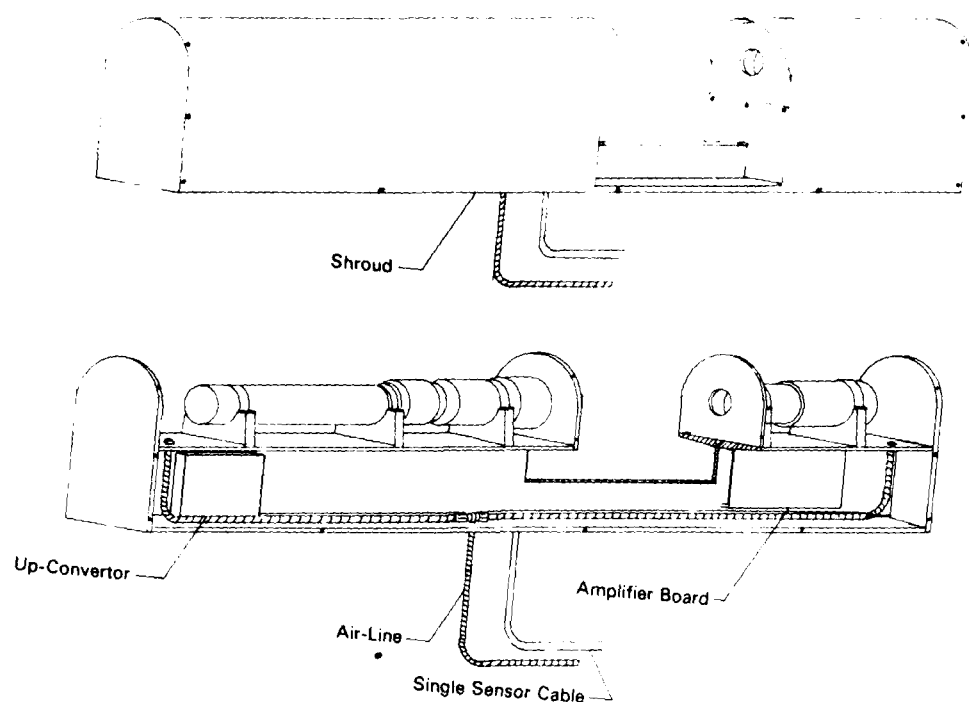


Fig. 11 — Concept of FSM after implementation of recommendations

## ACKNOWLEDGMENTS

We thank Ted Czuba for supporting the development of the Forward Scattering Meter as part of the SMOOS project (Project No. 63207N PDW106-8-058C-6X0514) of NAVAIR. We thank Gene Mack and Bruce Wattle of Calspan Corporation for their help in the testing and calibration of the FSM and for the use of their atmospheric test chamber. We also thank George D. Robertson and Kenneth L. Nicodemus of the Naval Research Laboratory's machine shop for their help in constructing the FSM.

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2. H. Gerber, "Liquid Water Content of Fogs and Hazes from Visible Light Scattering," *J. Climate and Appl. Meteor.* **23**, 1247-1252 (1984).
3. H.C. Van De Hulst, *Light Scattering by Small Particles* (Academic Press, New York, 1957).
4. H. Gerber, "Infrared Aerosol Extinction from Visible and Near-infrared Light Scattering," *Appl. Opt.* **24** 4155-4166 (1985).
5. Keithley Model 195T Instruction Manual, Document No. 195A-901-01A, Mar. 1984.

## APPENDIX A—SPECIFICATIONS

1. Display  
Six .5-in. LED digits with decimal point, exponent, and polarity. Function and IEEE-488 bus status are also displayed.
2. Warm-up  
1 hour to rated accuracy
3. Operating Environment  
-20° to 50° C 0 to 100% relative humidity
4. Power  
110 Vac/60 Hz    5 A maximum on air compressor circuit  
                         3 A maximum on electronics circuit
5. Connectors  
Electrical  
Bendix weatherproof connectors olive drab anodized  
Air line  
Red and blue anodized aluminum
6. Dimensions  
Sensor  
55L × 5W × 10H (in.)    Weight 30 lb  
Electronics enclosure  
24L × 20D × 10H (in.)    Weight 50 lb
7. Cables  
Detector/Reference and Reference/Chopper  
Shielded individual pairs 20 ft long  
Laser Power  
RG/213 Coaxial            20 ft long  
Air Line  
#6 Braided Stainless Steel Tubing 20 ft long  
AC Power Cable  
3 Conductor 18 Gage    30 ft long  
GPIB Cable  
24 Conductor 24 Gage    30 ft long
8. Weatherproofing  
Enclosure  
Solid Seam-Welded Stainless Steel  
Gasketed Cover  
White Polyurethane Based Paint  
Sensor  
Gasketed End Caps  
Gasketed Laser Tube  
Baffled Laser Opening  
Cleaning Air Flushing System  
White Polyurethane Based Paint

9. Measurement Capability

Capable of measuring forward scattered light between one part per one hundred and one part per one hundred thousand of the direct laser intensity, and of giving the infrared aerosol extinction coefficient,  $\sigma e$ , at about the 11- $\mu\text{m}$  wavelength by use of the scaling relationship:

$$\sigma e = AF$$

where  $A$  is a system constant and  $F$  is the fraction of scattered light.

# APPENDIX B—PARTS LIST

Item	Part#	Desc.	Quant.	Manufacturer
1.	TBF-22-11PS	Thru-bulkhead conn.	1	Bendix corp.
2.	TBF-14S-6PS	Thru-bulkhead conn.	2	Bendix corp.
3.	10-40450-14	Plain flat gasket	9	Bendix corp.
4.	10-40450-22	Plain flat gasket	6	Bendix corp.
5.	10-40450-10SL	Plain flat gasket	2	Bendix corp.
6.	10-40450-28	Plain flat gasket	2	Bendix corp.
7.	10-72814-6P	90° plug	2	Bendix corp.
8.	10-72822-11P	90° plug	1	Bendix corp.
9.	MS3106R14S-6S	Straight plug	2	Bendix corp.
10.	MS3106R22-11S	Straight plug	1	Bendix corp.
11.	10-72614-14S-6S	Straight plug	1	Bendix corp.
12.	10-72614-14S-6P	Straight plug	1	Bendix corp.
13.	10-72622-22-11S	Straight plug	2	Bendix corp.
14.	10-72611-10SL-3S	Straight plug	1	Bendix corp.
15.	10-72628-28-12S	Straight plug	1	Bendix corp.
16.	MS3102R-14S-6P	Wall mount recept.	1	Bendix corp.
17.	MS3102R-14S-6S	Wall mount recept.	2	Bendix corp.
18.	MS3102R-22-11P	Wall mount recept.	1	Bendix corp.
19.	MS3102R-10SL-3P	Wall mount recept.	1	Bendix corp.
19.	MS3102R-28-12P	Wall mount recept.	1	Bendix corp.
20.	5 × 5 × .313 in.	Alum. H-beam	5'	Metal Goods Inc.
21.	1000203	4 × 4 in. Air filter	3	Aluminum Filter
22.	Model 4110	Phase sensitive detector	1	Evans Elec. Inc.
23.	Model 195T	Digital multimeter	1	Kiethly Inst.
24.	09-LCM-001	Laser collimator	1	Melles-Griot
25.	09-LSF-001	Spatial filter	1	Melles-Griot
26.	05-LPL-340	Laser power supply	1	Melles-Griot
27.	05-LHP-1121	Cylindrical laser head	1	Melles-Griot
28.	C30809	Silicon photodiode	1	RCA Semiconduct.
29.	DOA-P101-AA	Air compressor	1	Gast Pumps
30.	AF887	Pressure regulator	1	Gast Pumps

## JAMES AND GERBER

Item	Part#	Desc.	Quant.	Manufacturer
31.	K294	Repair kit	1	Gast Pumps
32.	B81339	300 Rpm synchronous motor	1	Teledyne Acoust.
33.	09-LSP-27	Pinhole assembly	1	Melles-Griot
34.	09-LAR-001	Adapter ring	1	Melles-Griot
35.	09-LSR-007	Focusing optics	1	Melles-Griot
36.	.1 m 400 Vdc	Motor capacitor	1	General Instr.
37.	6044	1/4-6 Pipe-flare conn.	3	Speed Unlimited
38.	1016	#6 Ninety degree conn.	4	Speed Unlimited
39.	1002	Straight female conn.	6	Speed Unlimited
40.	6102	#6 T connector	1	Speed Unlimited
41.	6035	#6 Flare union	2	Speed Unlimited
42.	#6	#6 Steel braid. tub.	20'	Speed Unlimited
43.	#6	#6 Steel braid. tub.	6'	Speed Unlimited
44.	LL-25-25-632.8	Laser Lenses	3	Optics for Res.
45.	45EB03	45 Vdc power supply	1	Acopian Corp.
46.		Collimator lens adaptor	1	NRL Machine Shop
47.		Detector tube	1	NRL Machine Shop
48.		Front detector housing	1	NRL Machine Shop
49.		Rear detector housing	1	NRL Machine Shop
50.		Front collar mount	1	NRL Machine Shop
51.		Rear collar mount	1	NRL Machine Shop
52.		Droplet guard	1	NRL Machine Shop
53.		Light trap	1	NRL Machine Shop
54.		Lens stop	1	NRL Machine Shop
55.		5/32-1 spacer	3	NRL Machine Shop
56.		1-in. lockring	2	NRL Machine Shop
57.		1-5/8-in. lockring	1	NRL Machine Shop
58.		1-in. baffle	2	NRL Machine Shop
59.		1-5/16-in. baffle	1	NRL Machine Shop
60.		5/8-1-in. spacer	1	NRL Machine Shop
61.		Field stop	1	NRL Machine Shop
62.		Detector cradle mount	2	NRL Machine Shop
63.		Detector tube end cap	1	NRL Machine Shop
64.	TIL78	Phototransistor	2	Diplomat Elect.
65.		Detector tube gasket	1	NRL Machine Shop
66.		Laser tube hinge	1	NRL Machine Shop

## NRL REPORT 8996

Item	Part#	Desc.	Quant.	Manufacturer
67.		Laser tube housing	1	NRL Machine Shop
68.		Laser end cap	1	NRL Machine Shop
69.		Laser collar mounts	2	NRL Machine Shop
70.		Collimator collar mount	1	NRL Machine Shop
71.		Rear baffle	1	NRL Machine Shop
72.		Baffle spacer	1	NRL Machine Shop
73.		Front baffle	1	NRL Machine Shop
74.		Laser beam chopper	1	NRL Machine Shop
75.		Chopper motor mount	1	NRL Machine Shop
76.		Rear cap gasket	1	NRL Machine Shop
77.		Sensor base	1	NRL Machine Shop
78.		Sensor mount	1	NRL Machine Shop
79.		Sensor vibration mount	1	NRL Machine Shop
80.		Sensor mount base	1	NRL Machine Shop
81.		Laser tube cradle mount	2	NRL Machine Shop
82.		$\pm 15$ V power supply	2	Acopian Corp.
83.		Laser lens extender	1	NRL Machine Shop
84.		Laser lens lock ring	1	NRL Machine Shop
85.		Filter cover	1	NRL Machine Shop
86.		Calibrator	1	NRL Machine Shop
87.		Beam splitter mount	1	NRL Machine Shop
88.		Chopper mount	1	NRL Machine Shop
89.		Chopper bearing	1	
90.		Chopper	1	NRL Machine Shop
91.		Chopper reflector	1	NRL Machine Shop
92.		Beam cube splitter	2	Melles-Griot
93.		3/8-in. Rubber Tubing	1'	
94.	LL-25-25-632.8	Detector lenses	3	Optics for Res.
95.	001-LQS-004	Collimator lens	1	Melles-Griot

## APPENDIX C—DRAWINGS

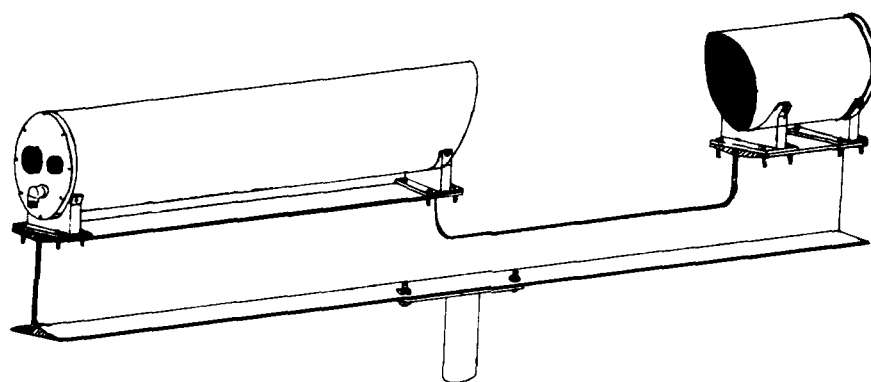
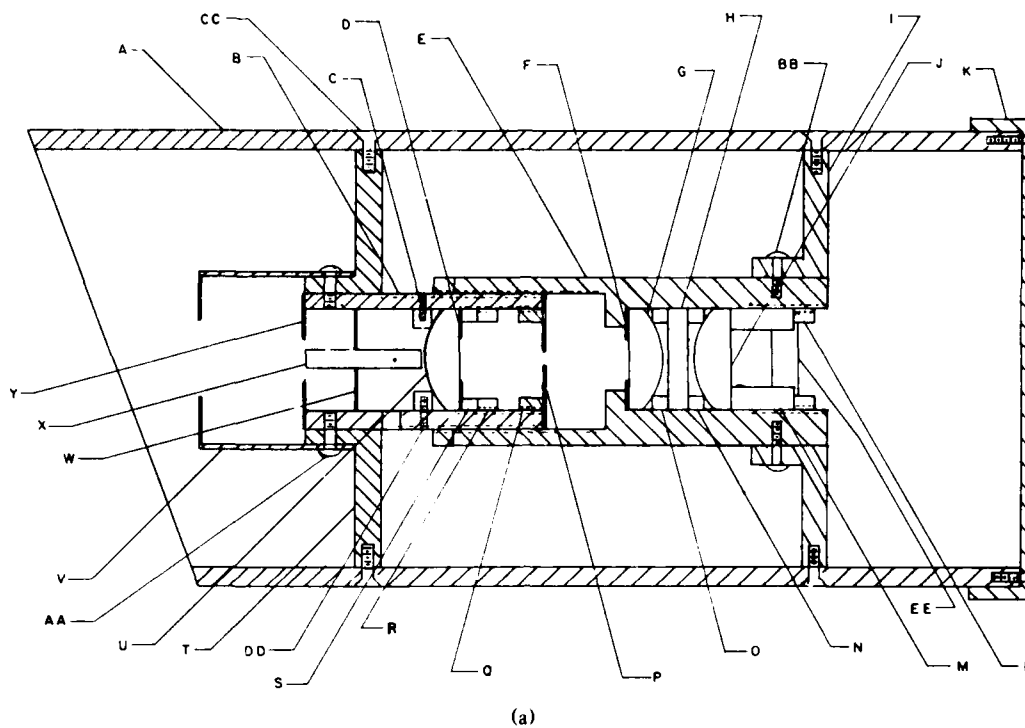


Fig. C1 — Forward Scattering Meter (FSM)

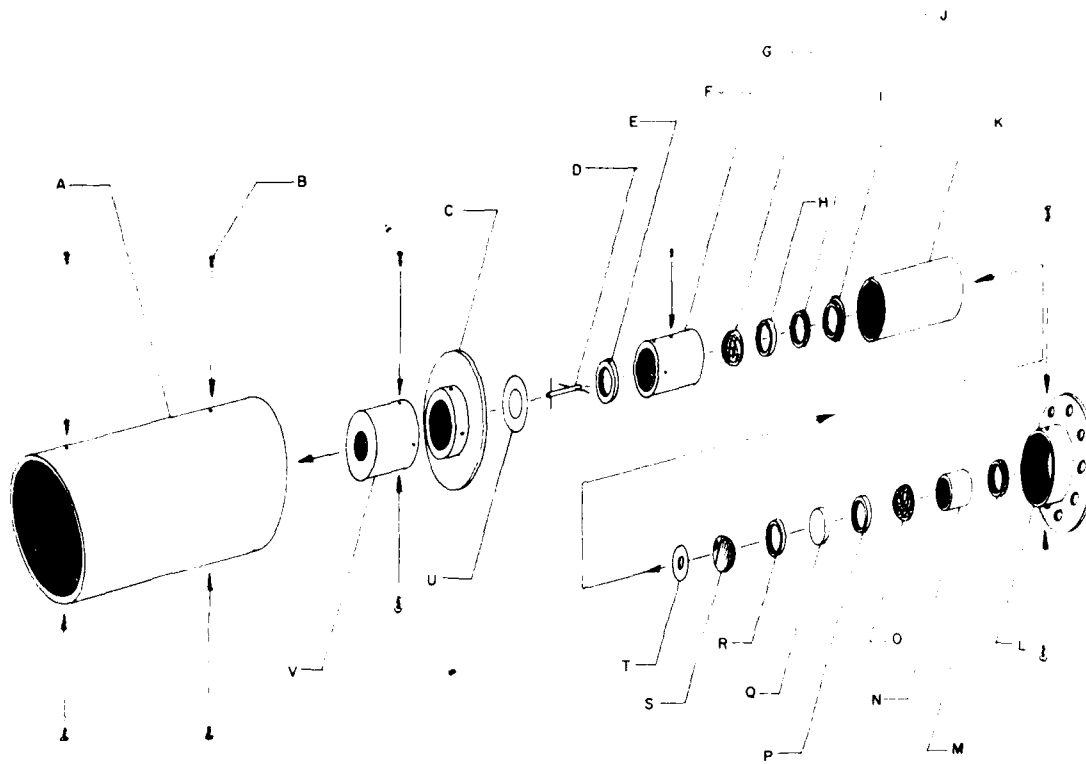


- (a)
- |  |  |
|--|--|
| A. Detector tube 4.5" O.D. 4.125" I.D. aluminum tubing | P. Detector threaded baffle aluminum bar stock               |
| B. Detector front housing aluminum bar stock           | Q. Detector threaded baffle aluminum bar stock               |
| C. Detector lens stop aluminum bar stock               | R. Detector locking aluminum bar stock                       |
| D. Detector front lens baffle aluminum shim stock      | S. Detector lens spacer aluminum bar stock                   |
| E. Detector rear housing aluminum bar stock            | T. Detector front collar mount aluminum bar stock            |
| F. Detector rear lens baffle aluminum shim stock       | U. Detector lens A   |
| G. Detector lens B                                     | V. Detector droplet cover aluminum bar stock                 |
| H. Detector filter                                     | W. Detector light trap mount piano wire                      |
| I. Detector rear collar mount aluminum bar stock       | X. Detector light trap 3/16" stainless steel thinwall tubing |
| J. Detector lens C                                     | Y. Detector front baffle aluminum shim stock                 |
| K. Detector tube cap aluminum bar stock                | AA. 4-40 round head screw                                    |
| L. Detector locking aluminum bar stock                 | BB. 4-40 round head screw                                    |
| M. Detector photodiode mount aluminum bar stock        | CC. 4-40 flat head screw                                     |
| N. Detector lens spacer aluminum bar stock             | DD. 4-40 set screw   |
| O. Detector lens spacer aluminum bar stock             |  |

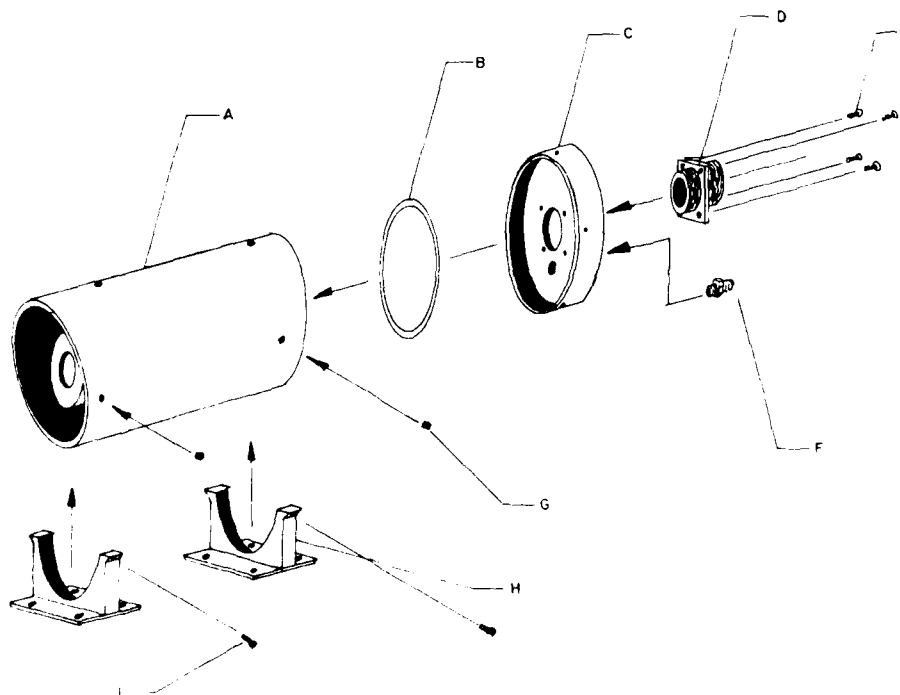
(b)

Fig. C2 — FSM detector; unless otherwise specified tolerances are  $\pm .002$ :  
(a) side section view and (b) parts list





(a)



(b)

Fig C3 — FSM detector: (a) exploded view and (b) assembly

1. Machine from 4 1/2" O.D. aluminum tubing with an I.D. of 4 1/8".
2. Black anodize and paint outer area with white polyurethane paint.

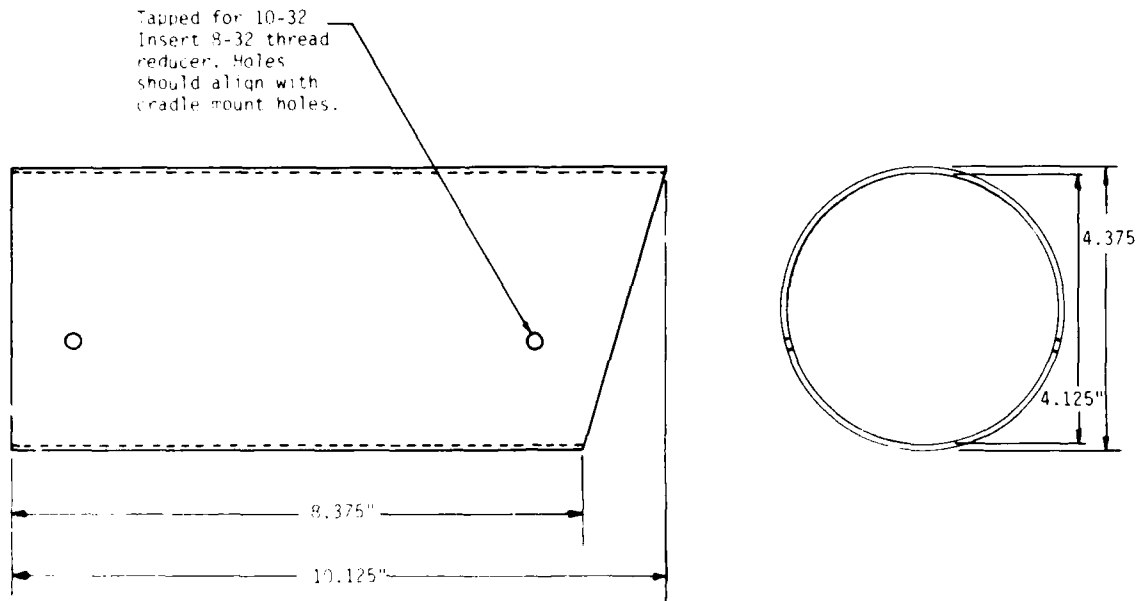


Fig C4 — FSM detector tube; unless otherwise specified, tolerances are  $\pm .02$

MATERIAL: 6061 T6 ALUMINUM

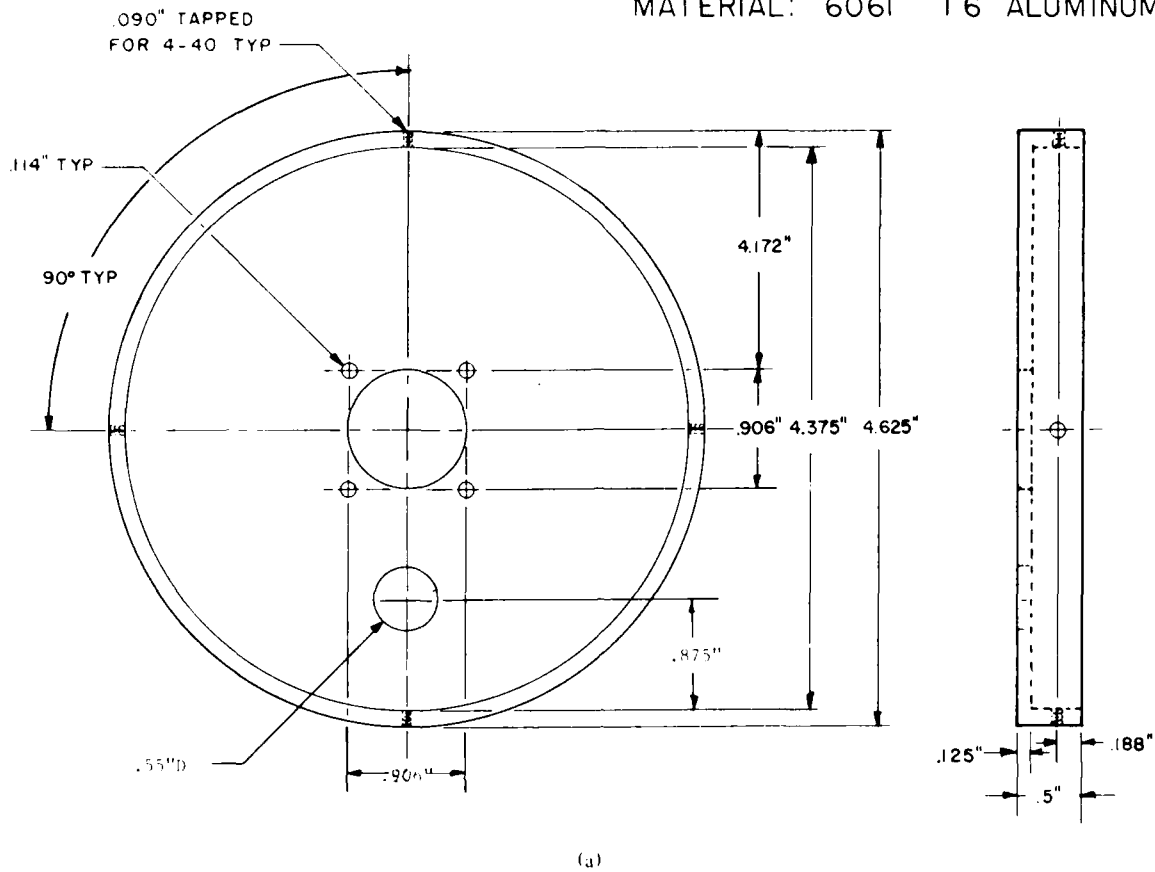


Fig C5 — FSM detector tube cap, unless otherwise specified, tolerances are  $\pm .002$   
 (a) front and side views and (b) notes

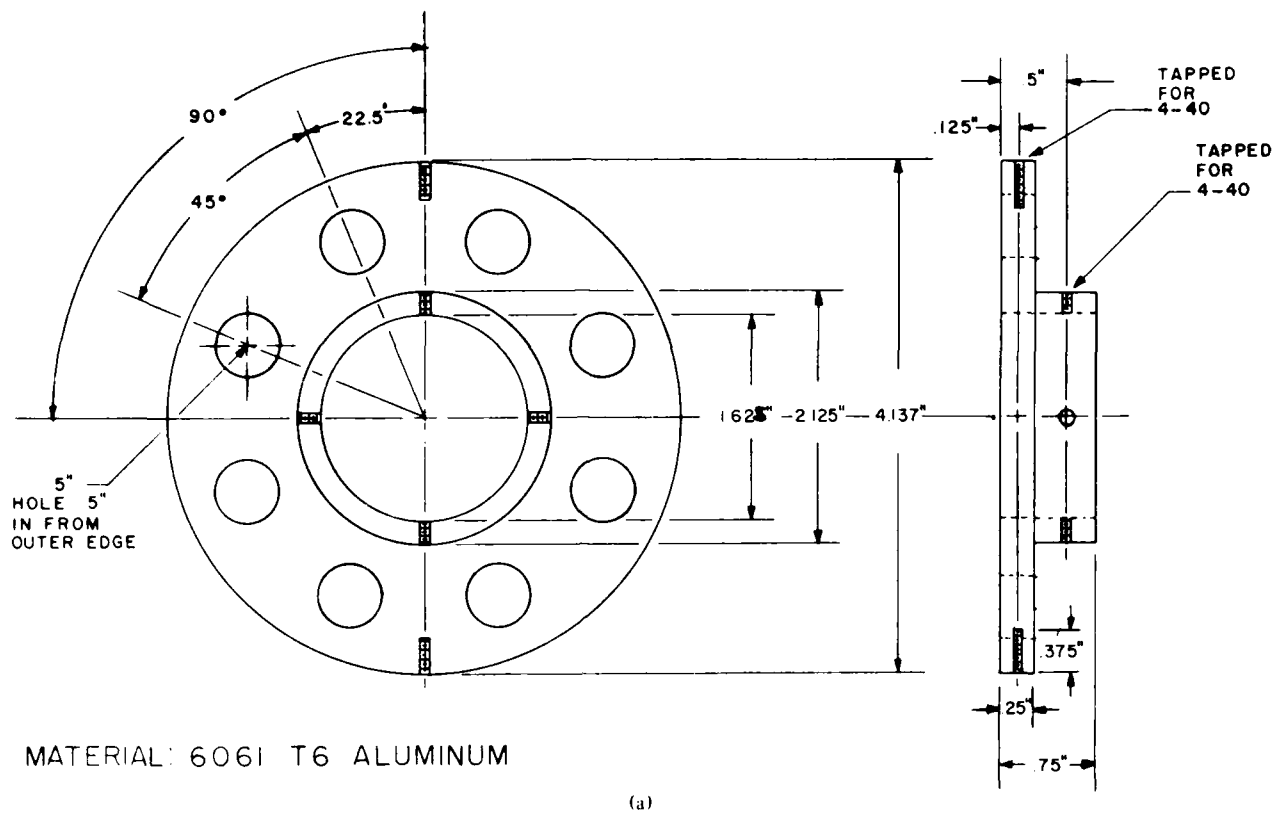
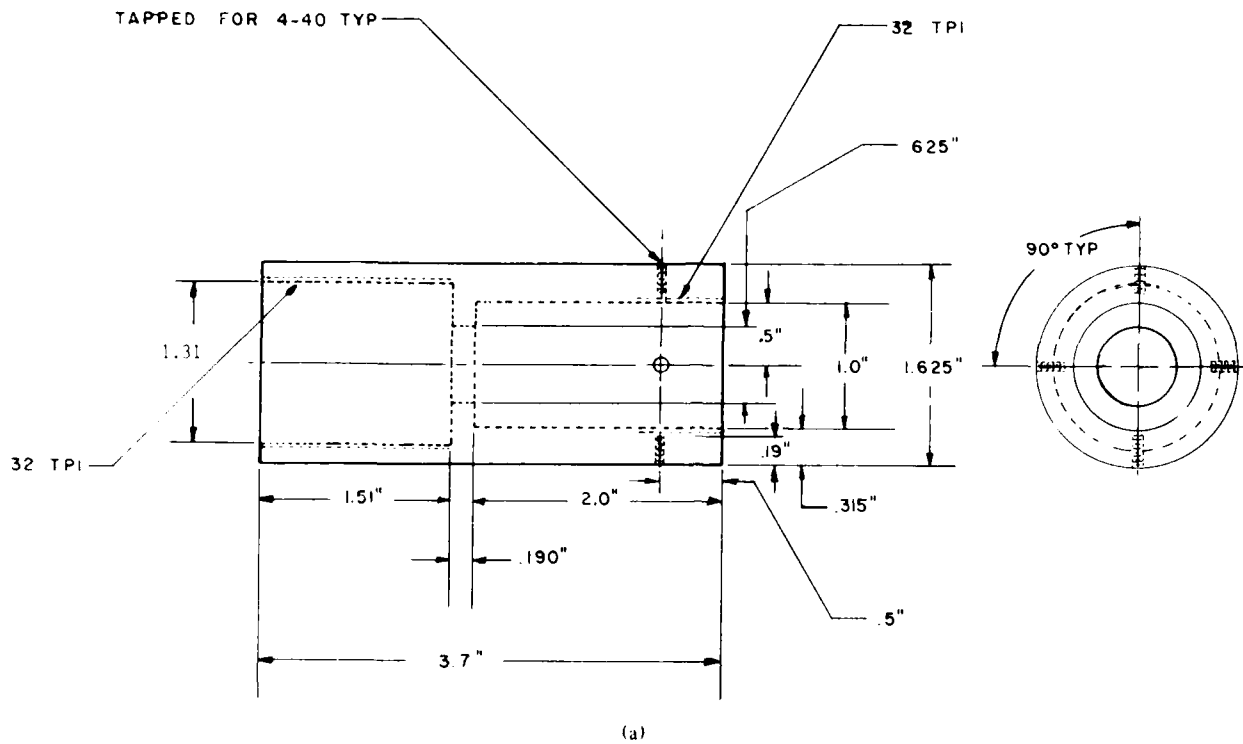


Fig. C6 — FSM detector; unless otherwise specified, tolerances are  $\pm .002$ :  
(a) collar mount and (b) notes

MATERIAL: 6061 T6 ALUMINUM



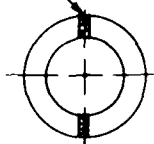
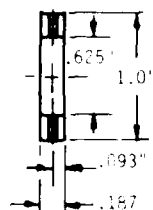
1. Machine to specified dimensions and tolerances from 1.75" aluminum bar stock.
2. Tolerance for the 1.0" inner diameter is  $+.002 \text{ } -.000$ .
3. Outer diameter of piece must be sliding fit with inner diameter of detector collar mount.
4. Piece must be free from burrs and sharp edges.
5. All dimensions are after finish.
6. *Black anodize after machining.*
7. Piece should have fine finish and overall good appearance.

(b)

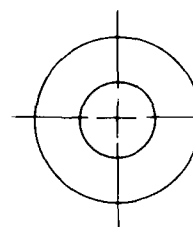
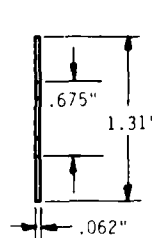
Fig C7 — FSM detector rear housing; unless otherwise specified, tolerances are  $\pm .002$   
 (a) side and front views and (b) notes

1. Machine from aluminum bar stock. 6061 T6
2. Black anodize.

Tapped for 4-40



1. Machine or cut from aluminum shim stock no thicker than 1/32".
2. Put knife-edge cut on I.D. of baffle.
3. Black anodize.



Lens stop

Baffle

- 3/16" hole,  
tapped to a  
circular pattern to  
allow air to  
pass to front  
leg.

1. Machine from aluminum bar stock.
2. Black anodize.
3. All measurements after finish.

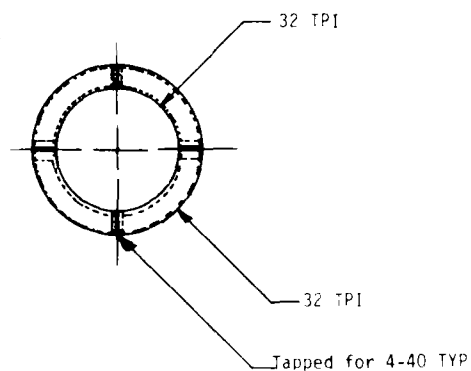
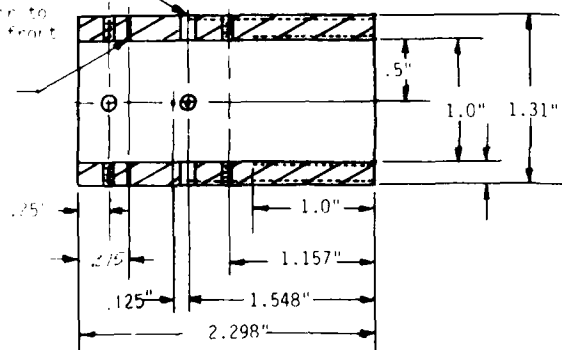
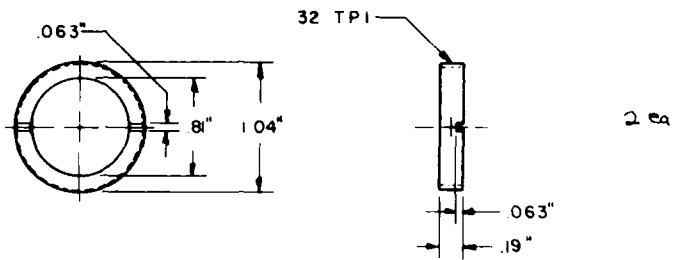
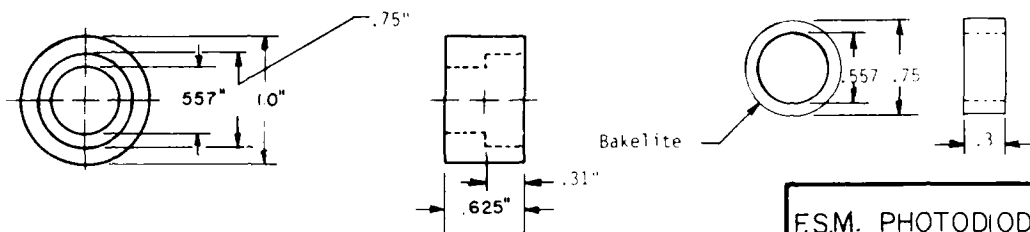


Fig. C8 — FSM detector front housing; unless otherwise specified, tolerances are  $\pm .002$



F.S.M. LOCKRING



F.S.M. PHOTODIODE MOUNT

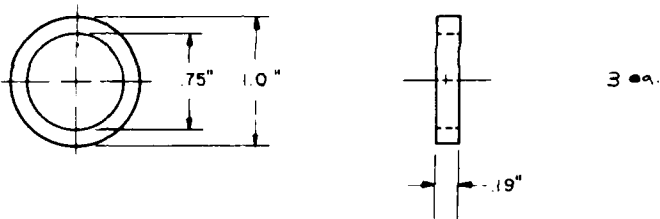


Fig C9 — FSM detector lens spacer, unless otherwise specified, tolerances are  $\pm .002$

1. Machine from aluminum bar stock (6061 T6 alloy or equivalent).
2. Should be good sliding fit with front detector collar mount.
3. Front opening should be cut to sharp edge.
4. Black anodize after finish.
5. All dimensions are after finish.

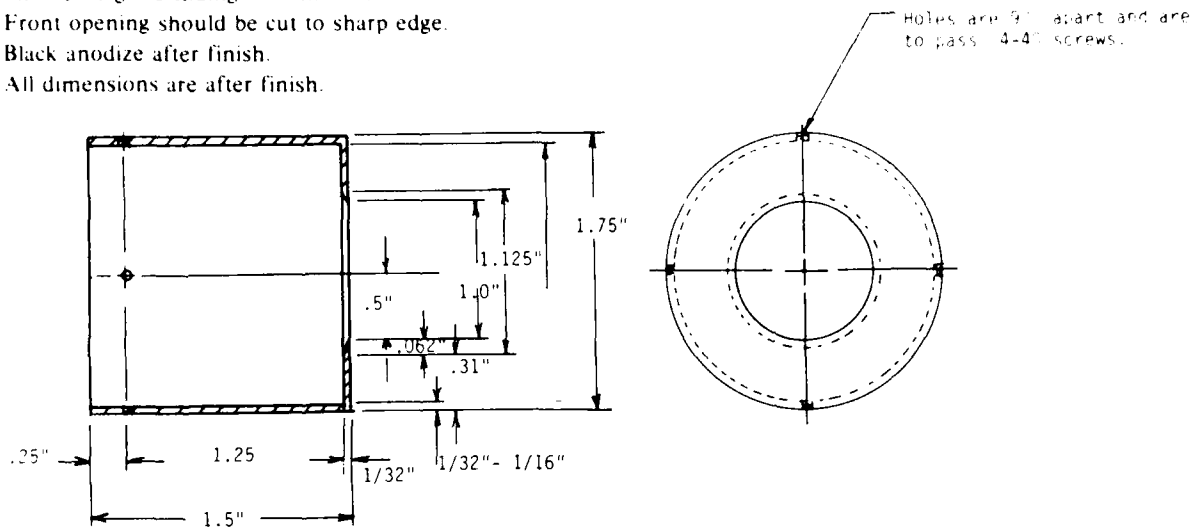


Fig. C10 — Detector droplet guard; unless otherwise specified, tolerances are  $\pm .002$

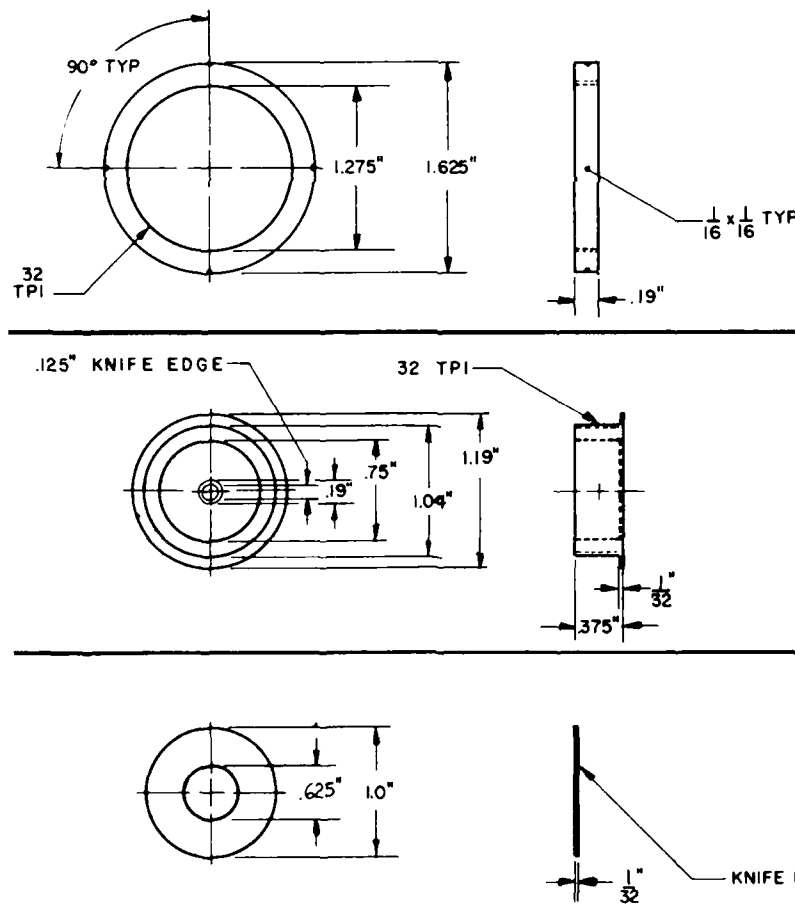


Fig. C11 — FSM detector; unless otherwise specified, tolerances are  $\pm .002$ : (a) front housing outer locking and (b) threaded baffle and (c) front lens baffle



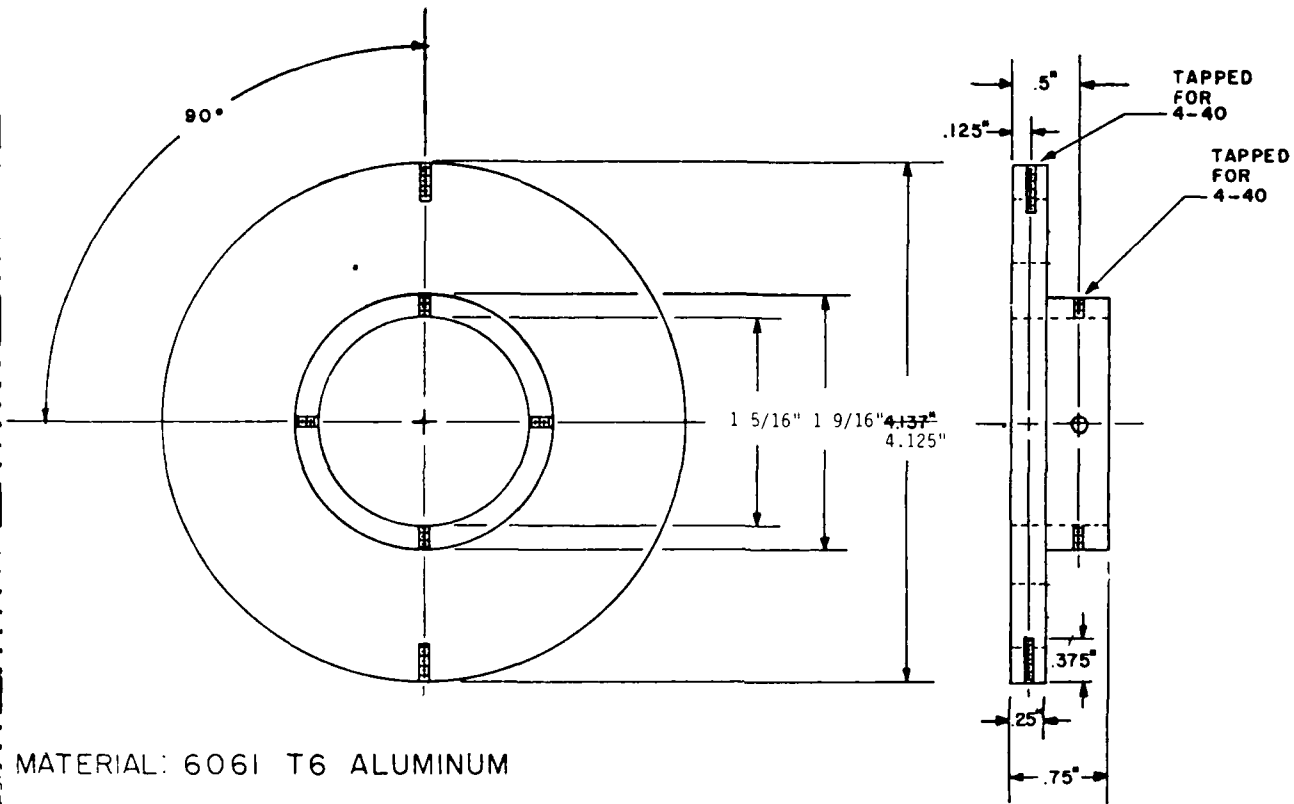


Fig. C12 — Detector front collar mount; unless otherwise specified, tolerances are  $\pm .002$

MATERIAL: 6061 T6 ALUMINUM

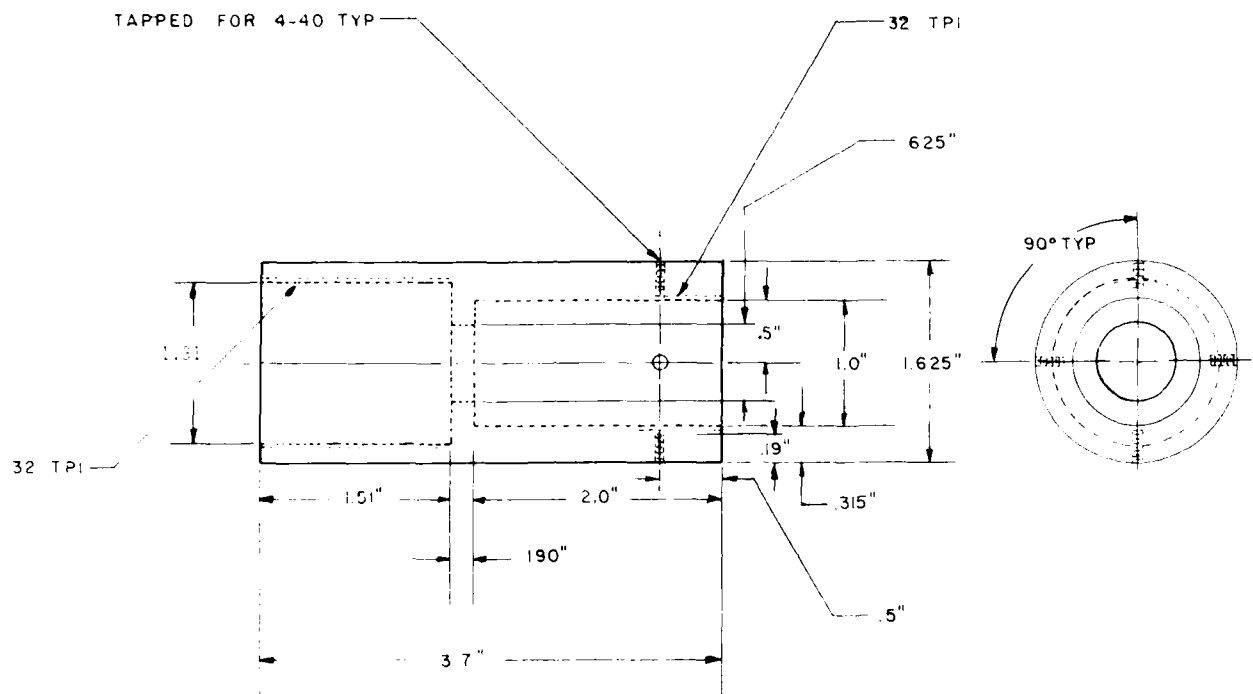
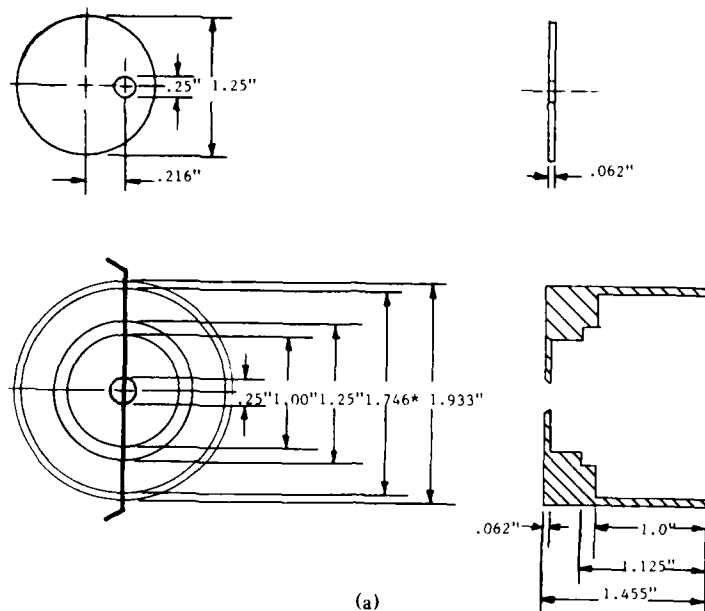


Fig. C13 — Detector rear housing, side and front views; unless otherwise specified, tolerances are  $\pm .002$

\*Must be good sliding fit with outer diameter of droplet guard.

1. Machine from 2" aluminum bar stock.
2. Piece must be free from all burrs and sharp edges.
3. All dimensions are after finish.
4. Black anodize.
5. Assemble as described on preceding figure.



1. Epoxy the ND3 filter in place.
2. Epoxy the cube beam splitter to the center of the cube beam splitter mount.
3. Epoxy the second cube beam splitter to the ND3 filter so it is aligned with the 1/4" hole in the ND3 filter as shown in the diagram.
4. Epoxy the cube beam splitter mount to the calibrator as shown.

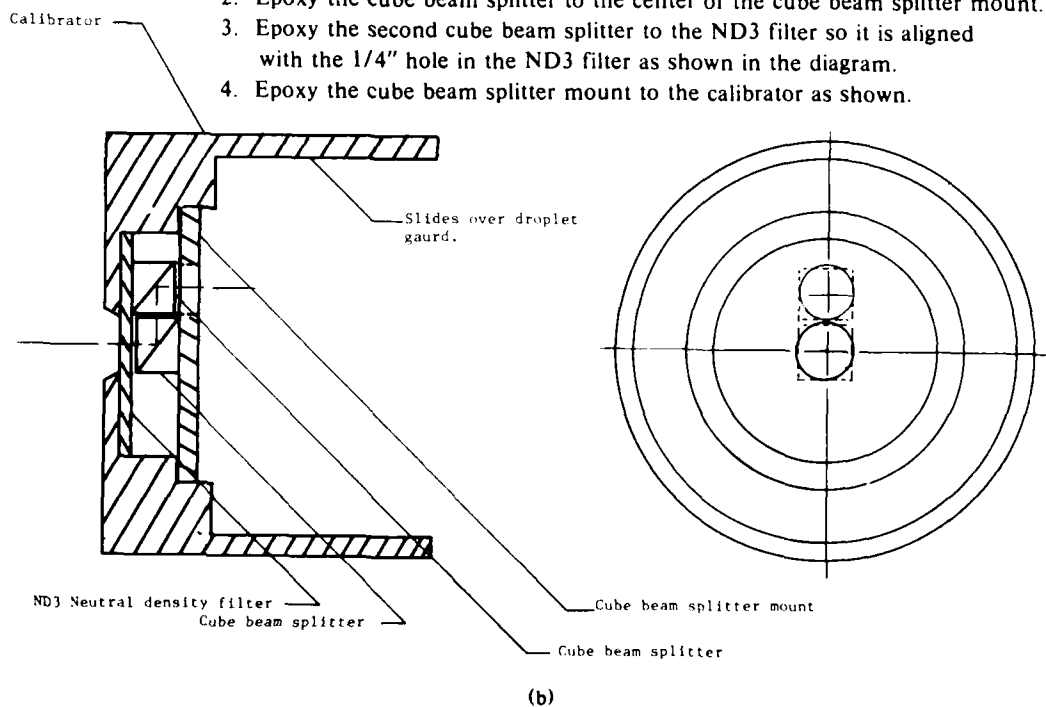


Fig. C14 — Calibration assembly; unless otherwise specified, tolerances are  $\pm .002$ .  
(a) front and side views and (b) assembly view

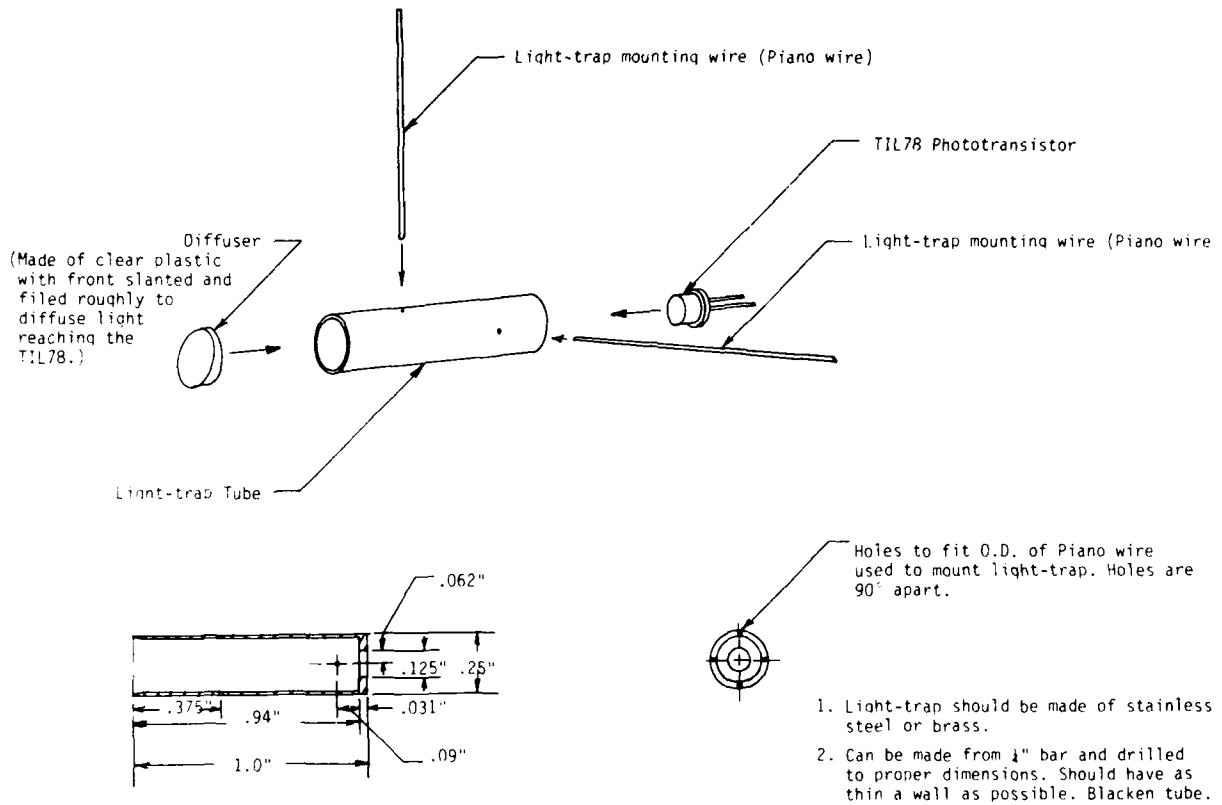
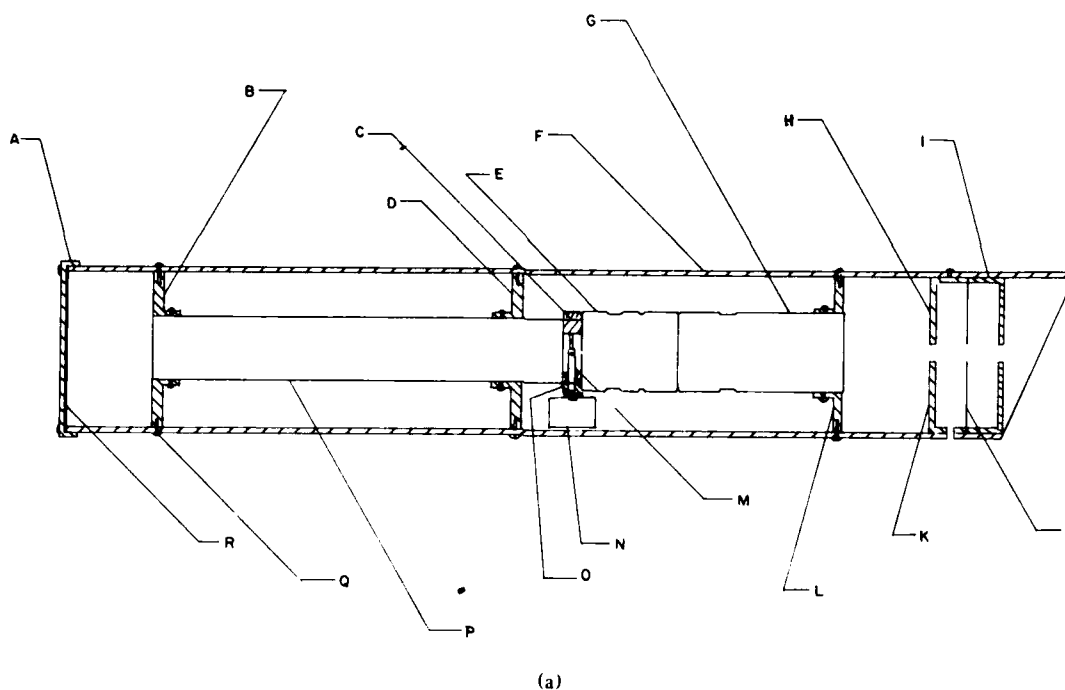


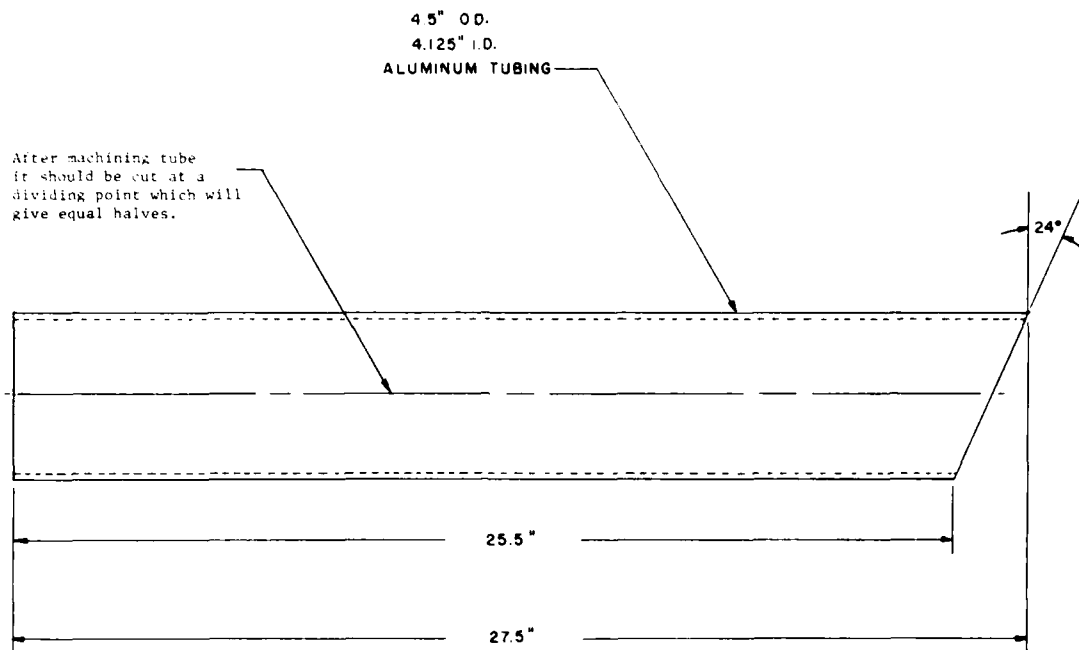
Fig. C15 — Light-trap dimensions and assembly, unless otherwise specified, tolerances are  $\pm .002$



- (a)
- A. Laser tube end cap 6061 T6 aluminum bar stock
  - B. Rear laser collar mount 6061 T6 aluminum bar stock
  - C. Modified Melles-Griot 09LAR001 adaptor ring
  - D. Front laser collar mount 6061 T6 aluminum bar stock
  - E. Melles-Griot spatial filter
  - F. Laser tube 6061 T6 aluminum tubing 4.5" O.D. 4.125" I.D.
  - G. Melles-Griot collimator
  - H. Laser cylinder baffle A 6061 T6 aluminum bar stock
  - I. Laser cylinder baffle B 6061 T6 aluminum bar stock
  - J. Laser cylinder spacer 1/16" aluminum sheet stock
  - K. Laser cylinder baffle A 6061 T6 aluminum bar stock
  - L. Collimator collar mount 6061 T6 aluminum bar stock
  - M. Chopper blade extension shaft 6061 T6 aluminum bar stock
  - N. 300 RPM chopper motor
  - O. Chopper motor mount 1/16"-3/32" aluminum sheet stock
  - P. Melles-Griot HeNe laser
  - Q. Stainless steel 1/2" 4-40 screw
  - R. Laser tube end cap gasket 1/16" neoprene rubber

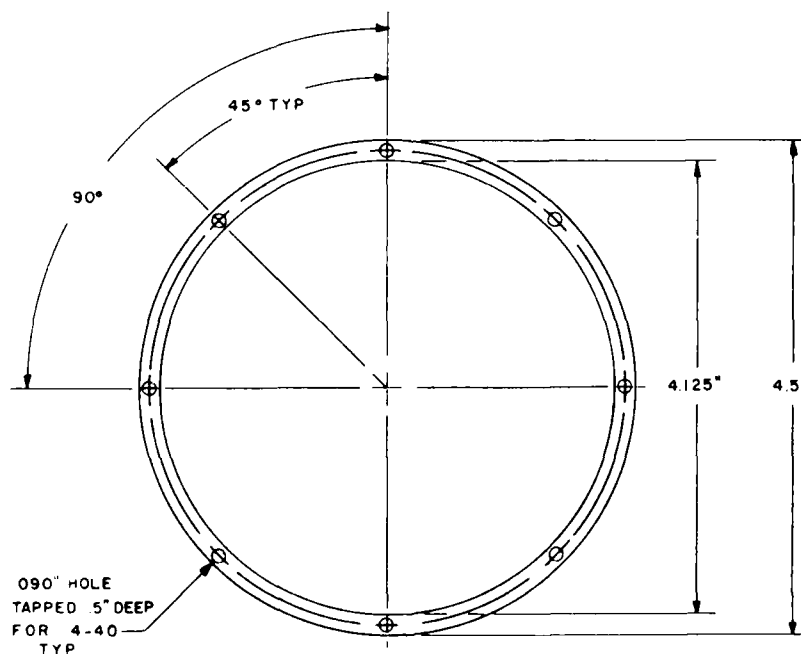
(b)

Fig. C16 — FSM laser assembly; unless otherwise specified, tolerances are  $\pm .002$ :  
(a) sectional side view and (b) parts list



MATERIAL: 6061 T6 ALUMINUM

(a)



MATERIAL: 6061 T6 ALUMINUM TUBING

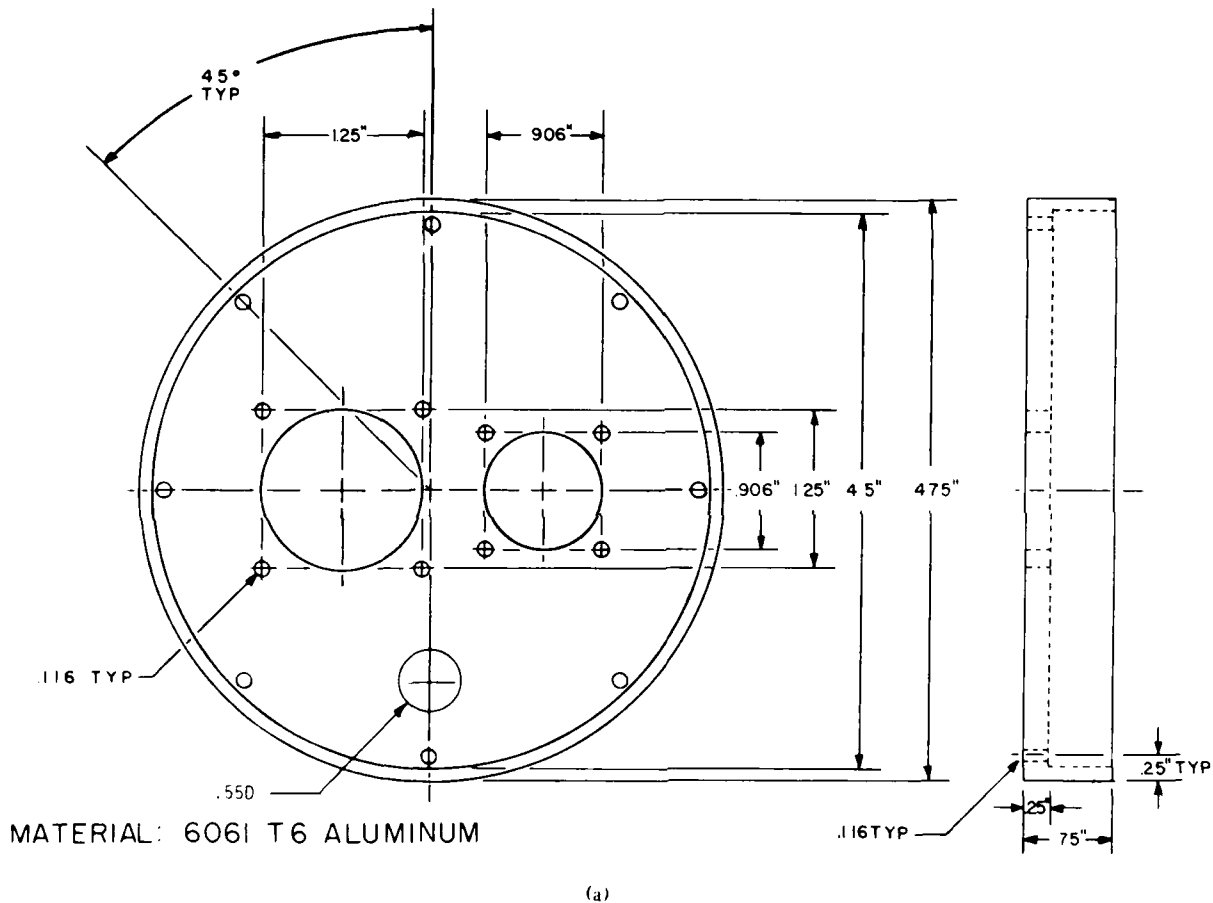
(b)

Fig. C17 — FSM laser tube; unless otherwise specified, tolerances are  $\pm .002$ :  
(a) side view, (b) rear view, and (c) notes

1. Cut and machine to specified dimensions and tolerances from 4-1/2" O.D. 4-1/8" I.D. aluminum tubing
2. Piece should be free from burrs and sharp edges.
3. Piece should have fine finish and overall good appearance.
4. All dimensions are after finish.
5. Black anodize after cutting and machining.
6. An aluminum hinge should be used to attach the two halves after being cut.
7. The hinge should be black anodized.

(c)

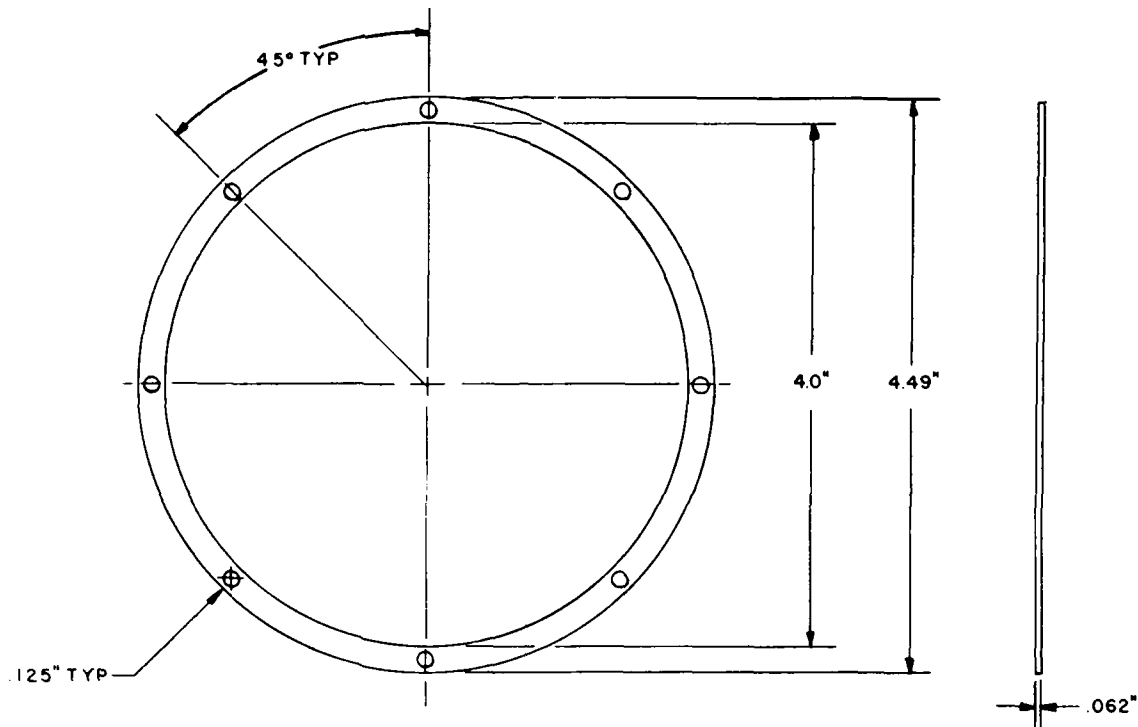
Fig C17 (Continued) — FSM laser tube; unless otherwise specified, tolerances are  $\pm .002$   
(a) side view, (b) rear view, and (c) notes



1. Machine to specified dimensions and tolerances from 5" aluminum bar stock.
2. Inner diameter of laser tube end cap should be sliding fit with outer diameter of detector tube.
3. Piece should be free from burrs and sharp edges.
4. All dimensions are after finish.
5. Black anodize after machining.

(b)

Fig C18 — FSM laser tube, unless otherwise specified, tolerances are  $\pm .002$   
(a) end cap and (b) notes



MATERIAL: .062" NEOPRENE

(a)

1. Cut to dimensions and tolerances specified from 1/16" neoprene rubber sheet.
2. Outer diameter of gasket must fit in laser tube cap.
3. Glue to inside of laser tube cap.

(b)

Fig. C19 — FSM laser tube; unless otherwise specified, tolerances are  $\pm .002$   
(a) cap gasket and (b) notes



1. Machine from 6061 T6 aluminum bar stock.
2. Two laser collar mounts are needed.
3. Black anodize.

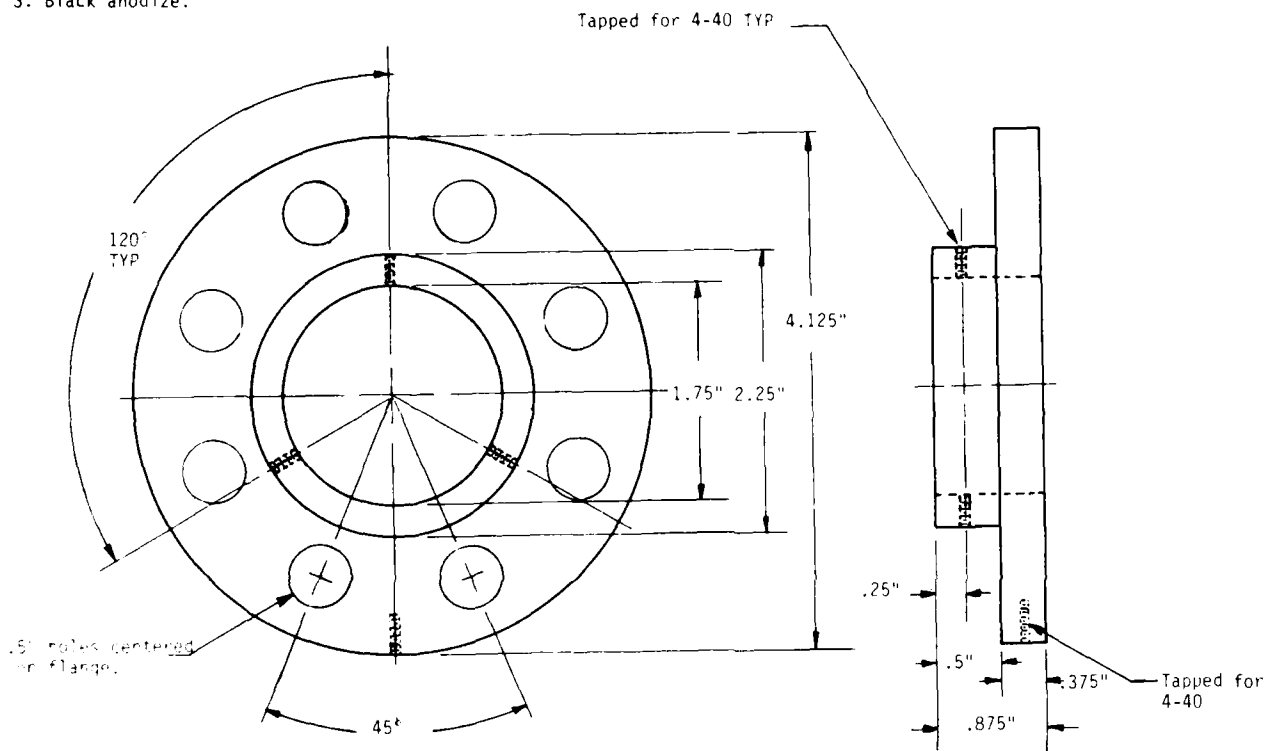


Fig C20 — Laser collar mount; unless otherwise specified, tolerances are  $\pm .002$

1. Machine from 4 1/4" aluminum bar stock.
2. Black anodize.

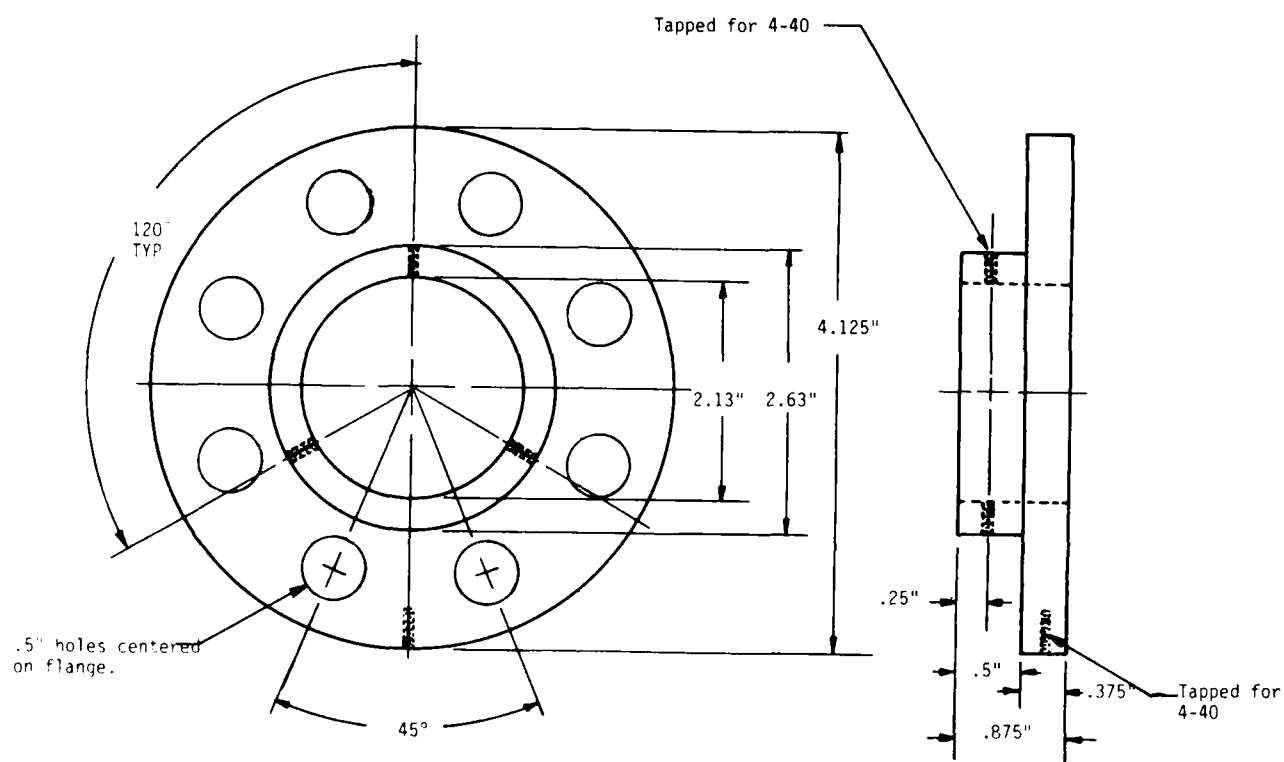


Fig. C21 — Collimator collar mount; unless otherwise specified, tolerances are  $\pm .002$

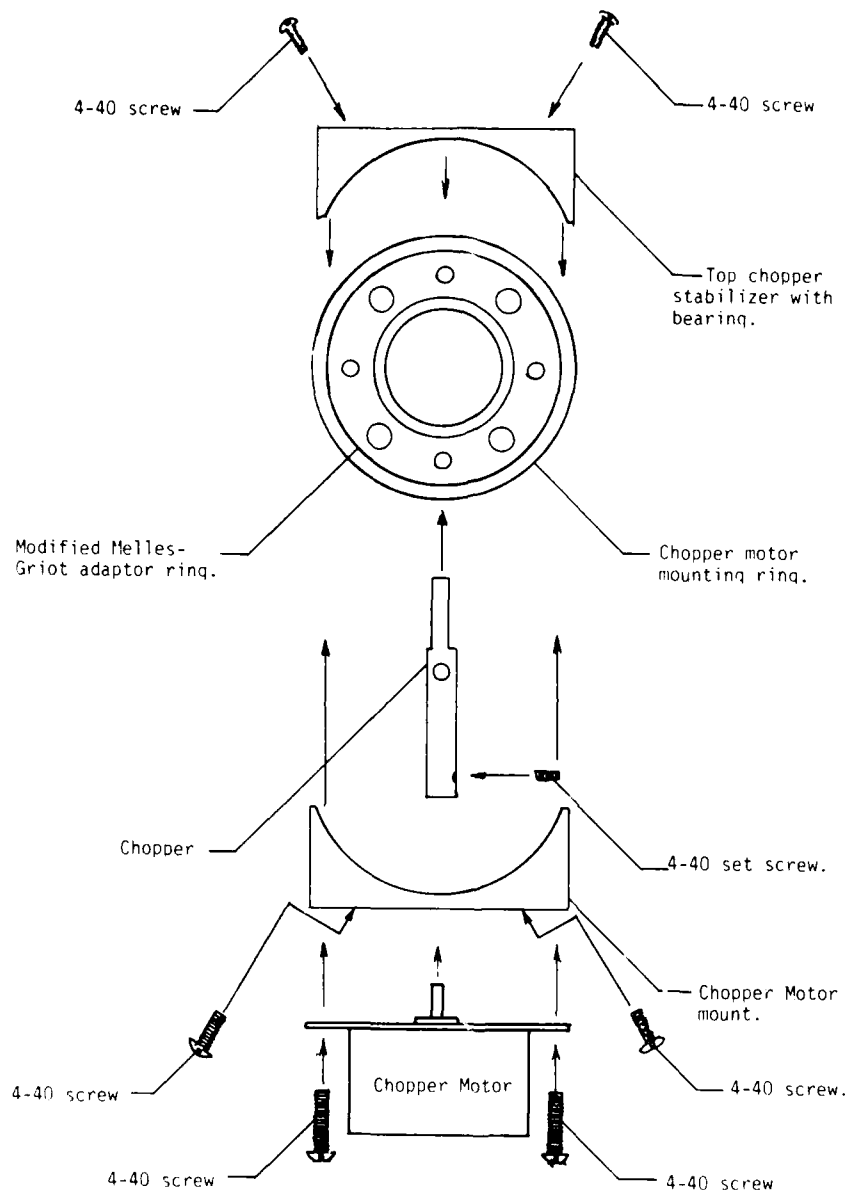


Fig. C22 — Assembly of chopper mount

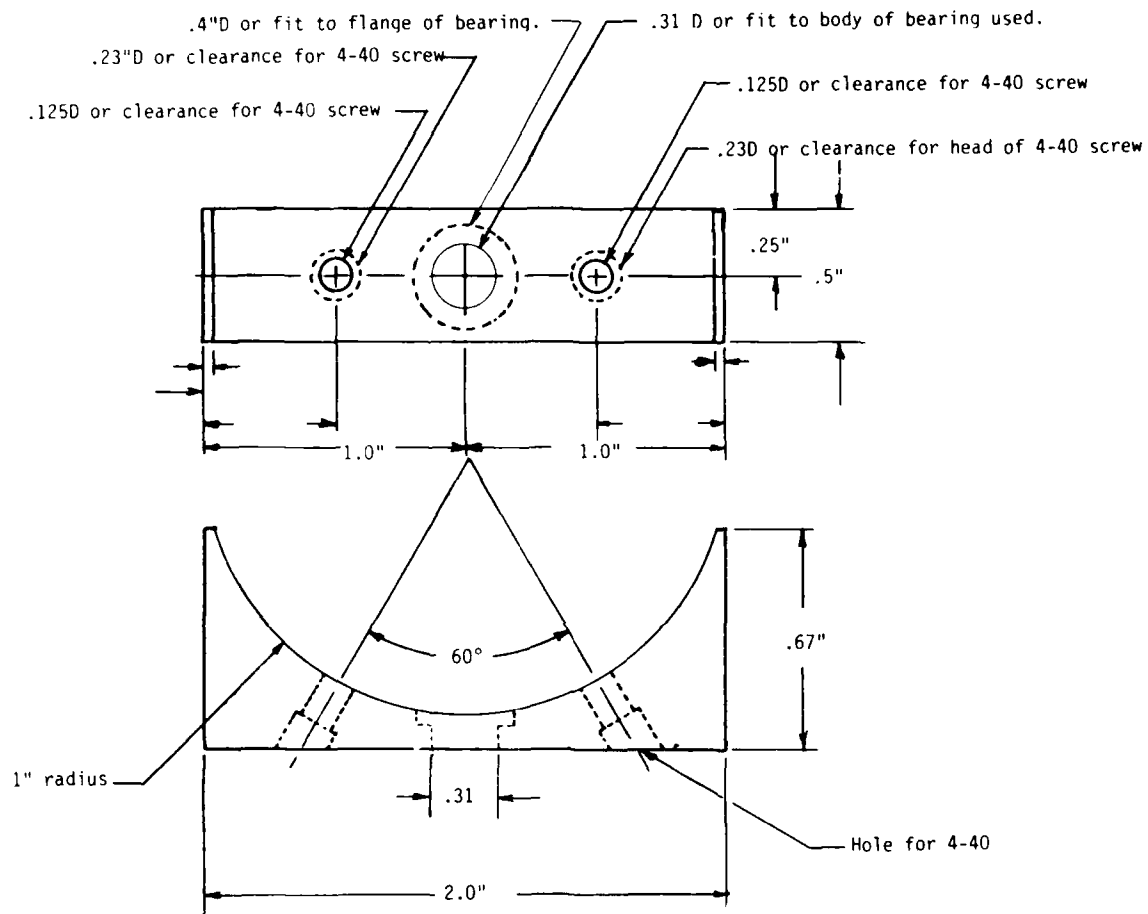


Fig. C23 — Chopper stabilizer; unless otherwise specified, tolerances are  $\pm .002$

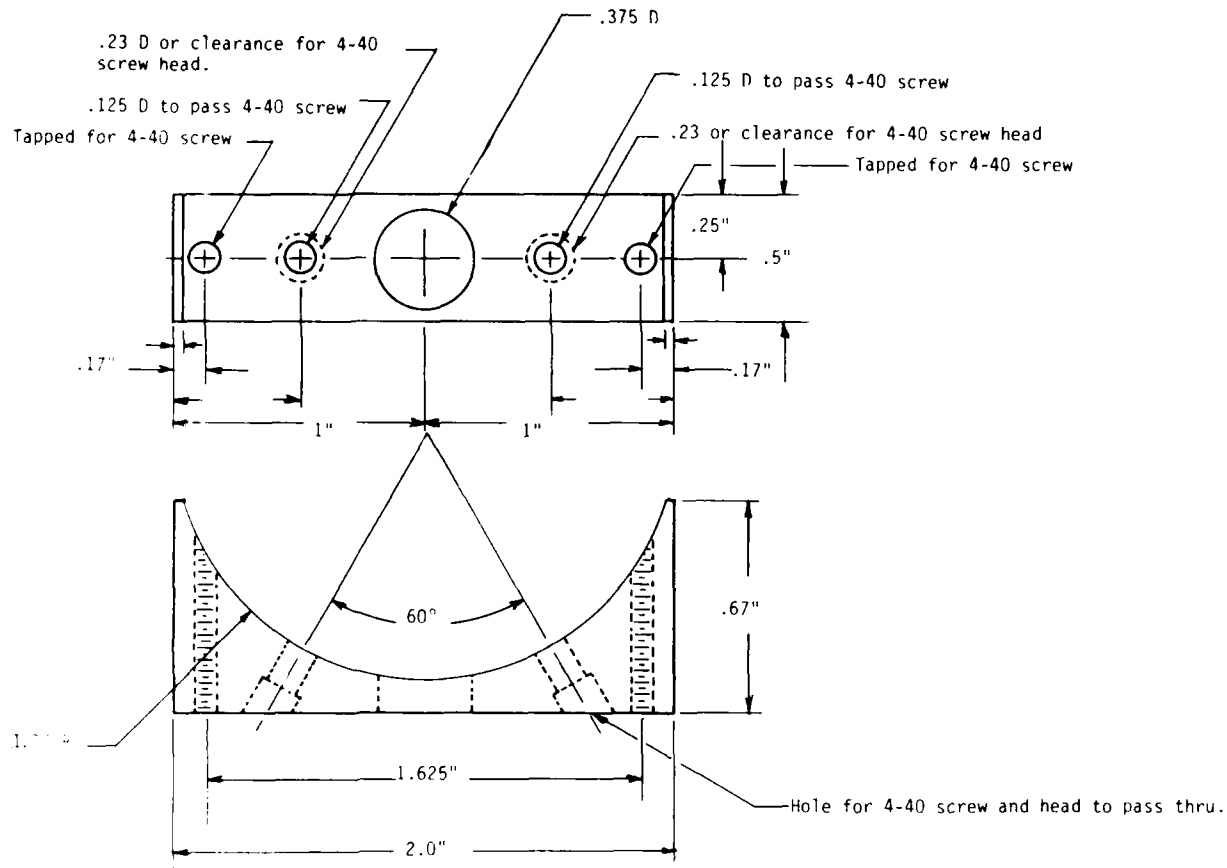


Fig. C24 — Chopper motor mount; unless otherwise specified, tolerances are  $\pm .002$

49

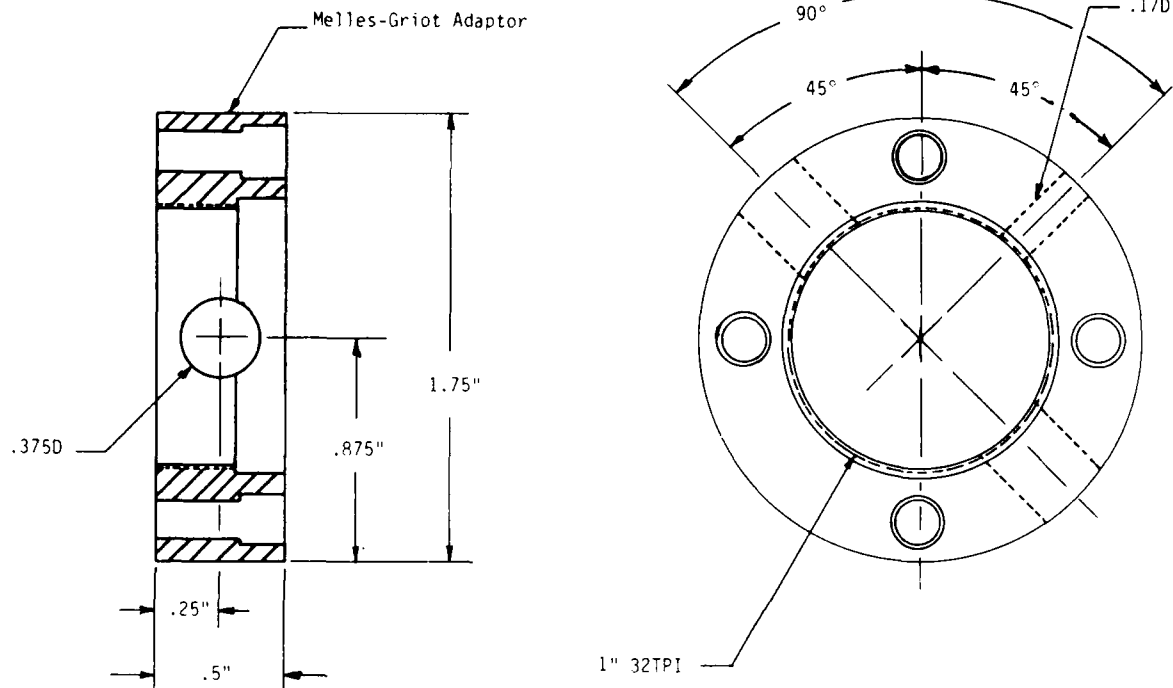


Fig. C26 — Modifications to the Melles-Griot adaptor; unless otherwise specified, tolerances are  $\pm .005$

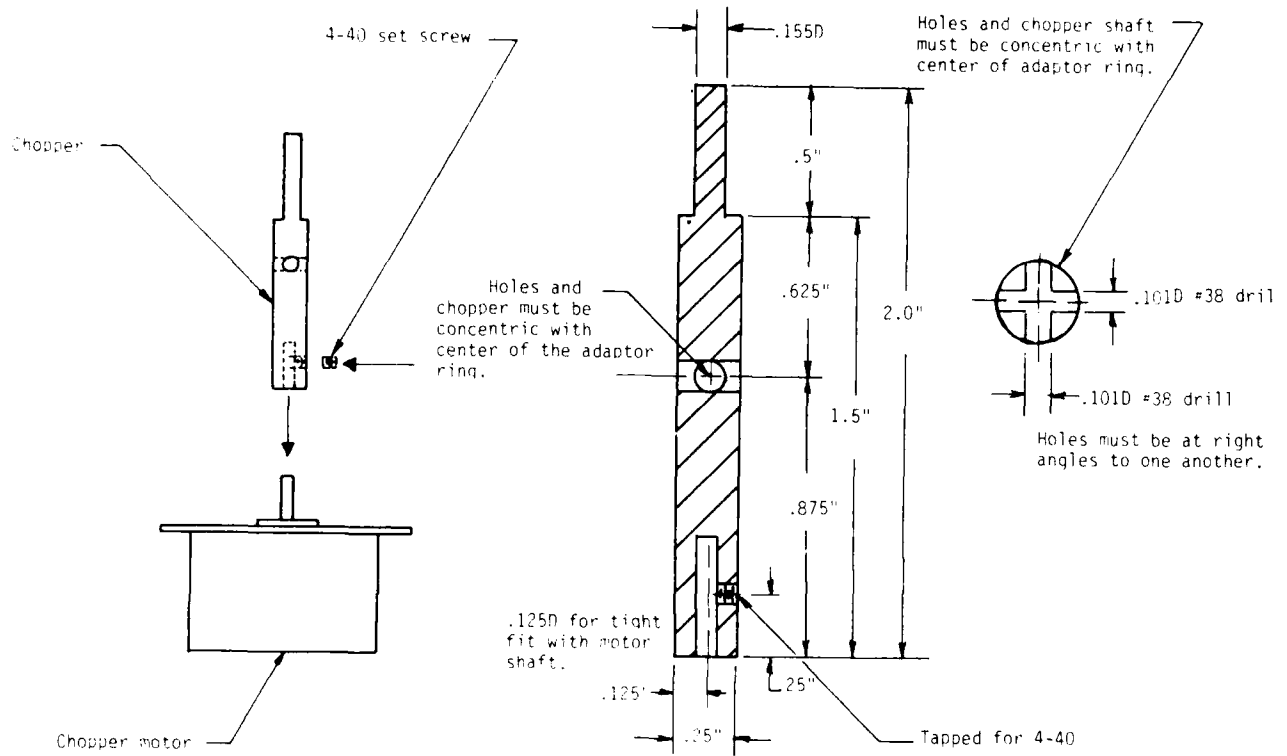
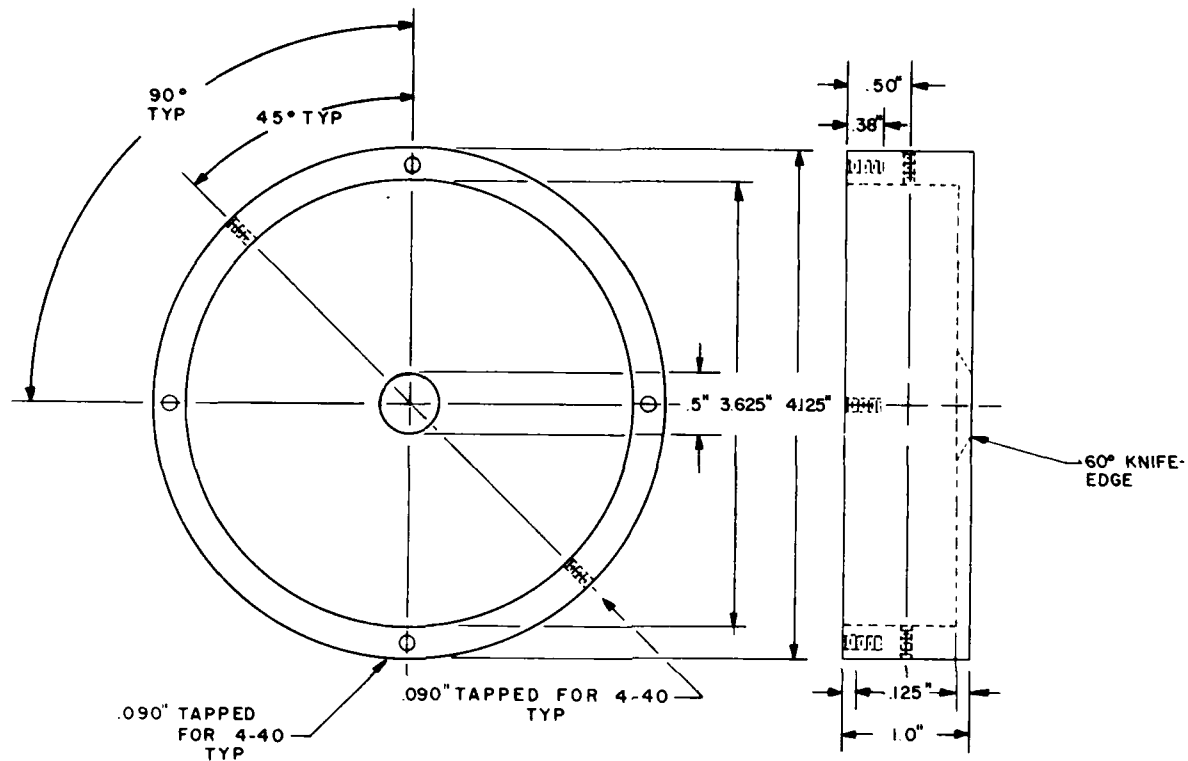


Fig. C27 — Chopper, unless otherwise specified, tolerances are  $\pm .002$





MATERIAL: 6061 T6 ALUMINUM

(a)

1. Machine 4.25" aluminum bar stock to specified dimensions and tolerances.
2. Outer diameter must be tight sliding fit with inner diameter of laser tube.
3. All dimensions specified are after finish.
4. Free all holes and edges from burrs and sharp areas.
5. Piece should have fine finish and overall good appearance.
6. Black anodize after machining.

(b)

Fig C28 — Laser cylinder, unless otherwise specified, tolerances are  $\pm .002$   
(a) baffle A and (b) notes

1. Machine or cut from 1/16" aluminum sheet
2. Black anodize.

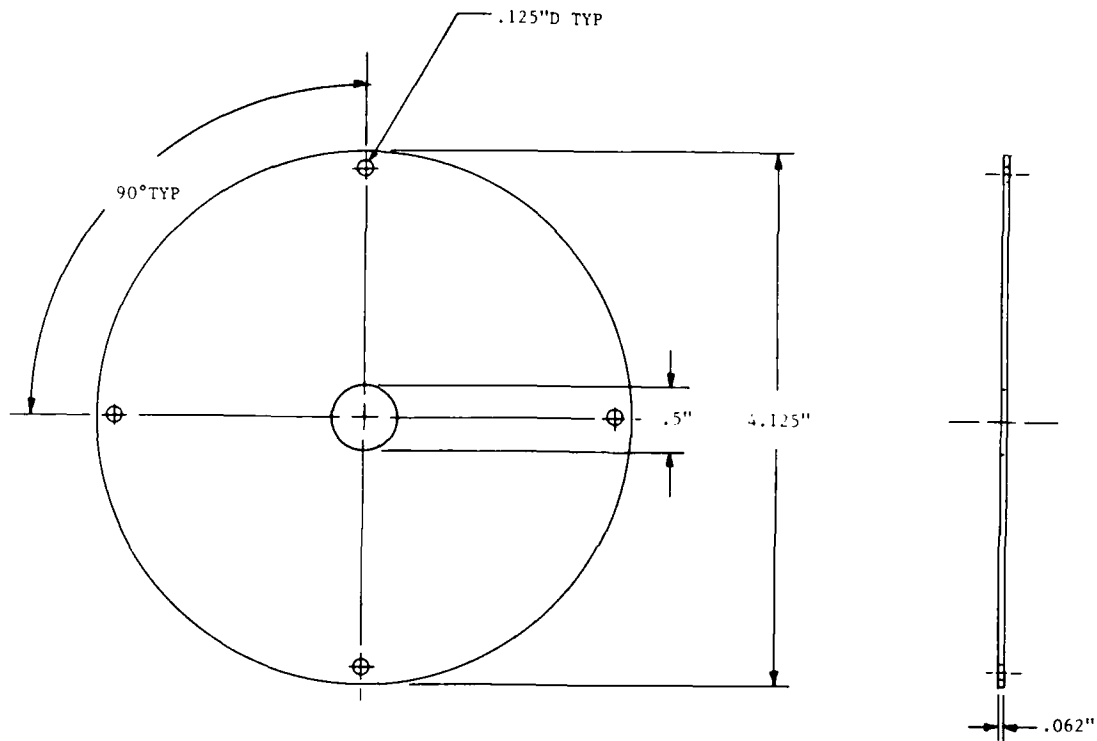


Fig. C29 — Laser tube baffle plate; unless otherwise specified, tolerances are  $\pm .002$

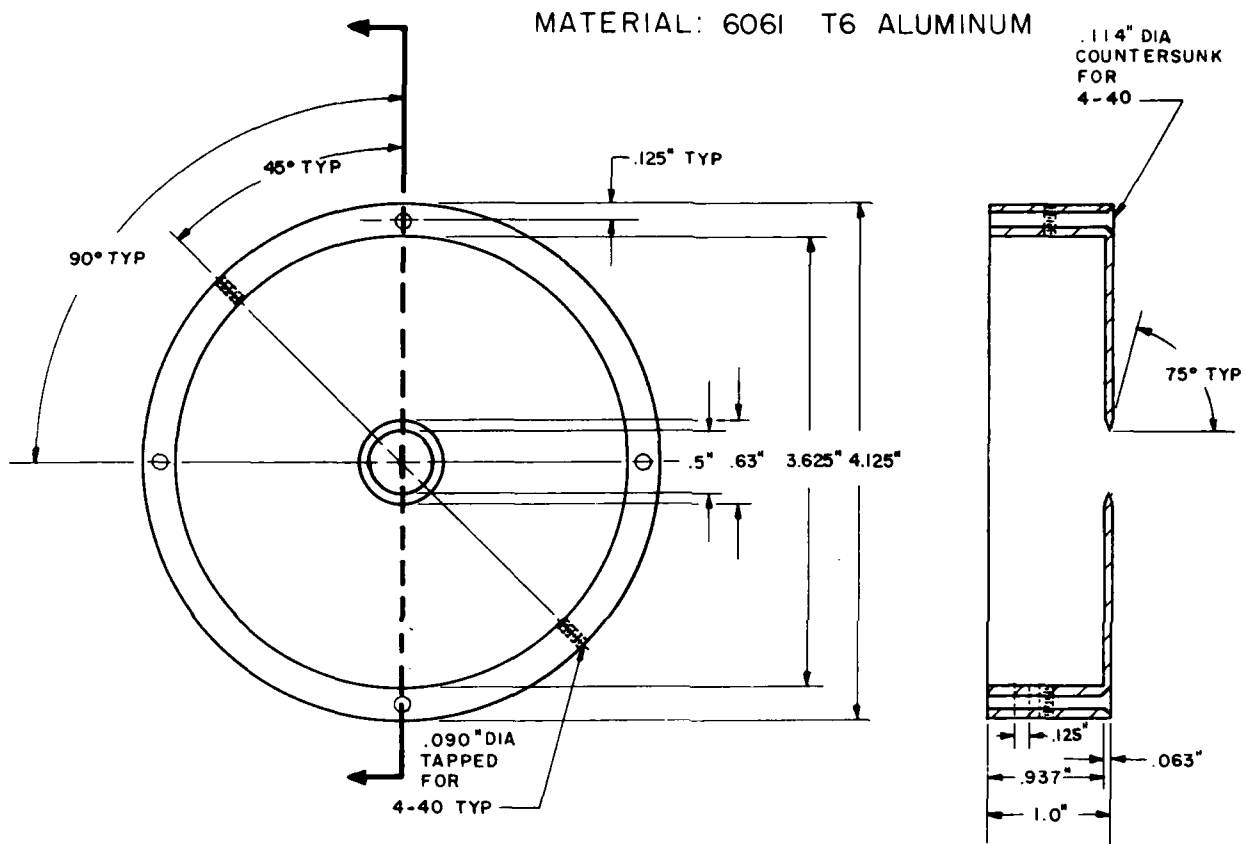


Fig. C30 — FSM laser baffle B; unless otherwise specified, tolerances are  $\pm .002$

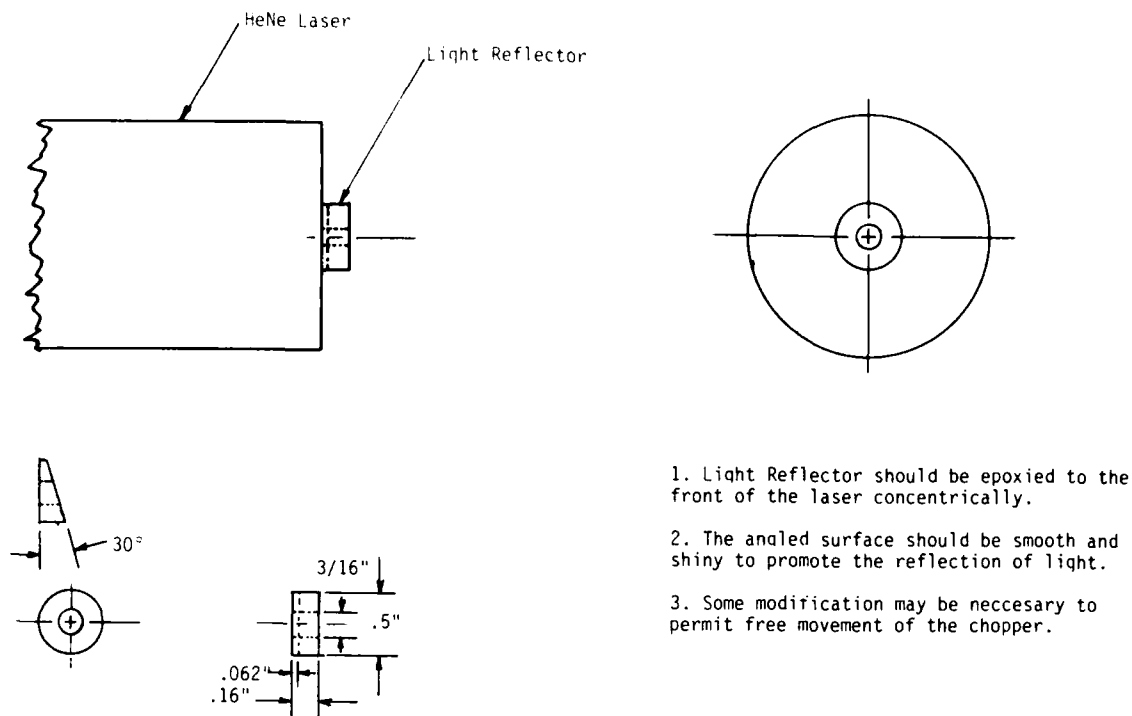


Fig. C31 — Light reflector; unless otherwise specified, tolerances are  $\pm .002$

1. Machine from aluminum bar stock.
2. Black anodize after finish.
3. All dimensions are after finish.

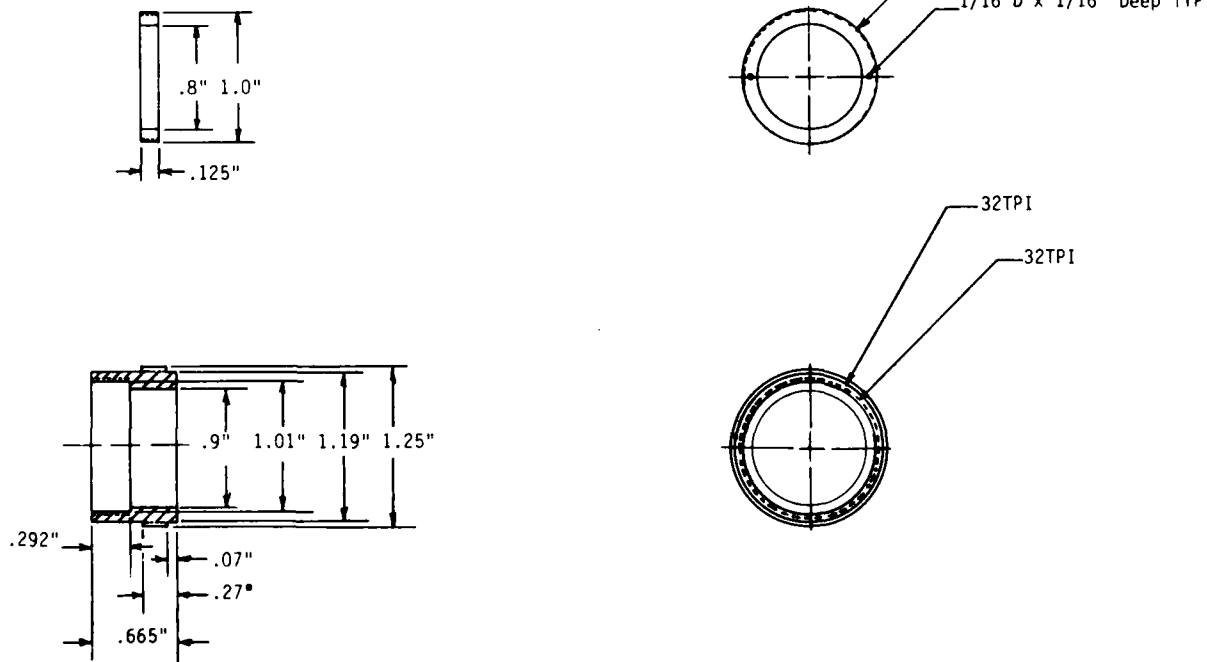


Fig. C32 — Collimator lens adaptor

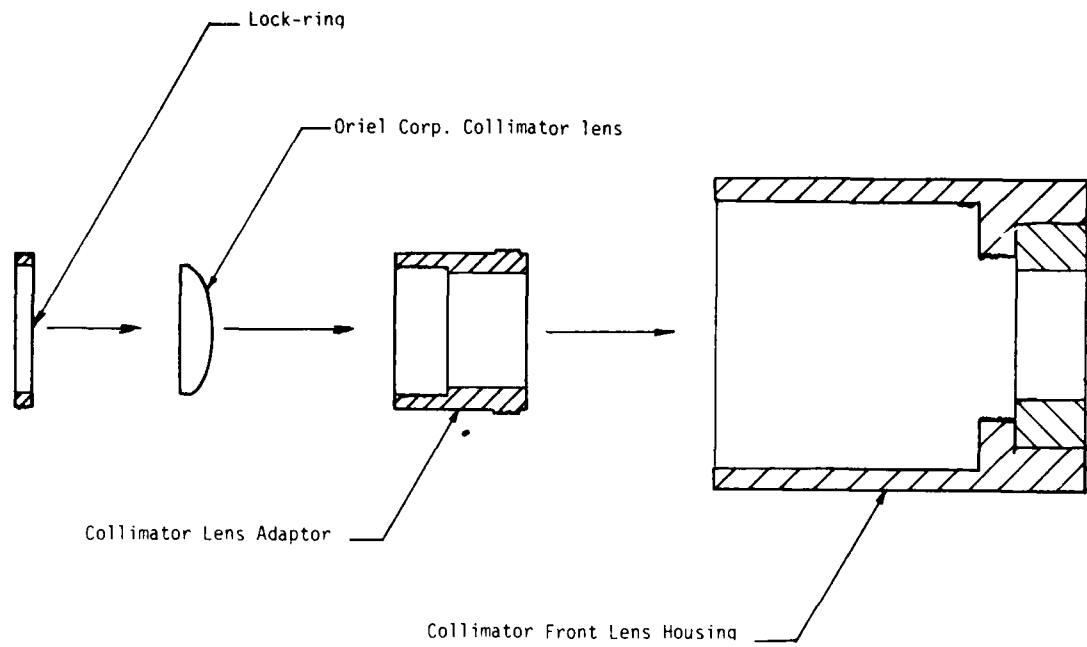
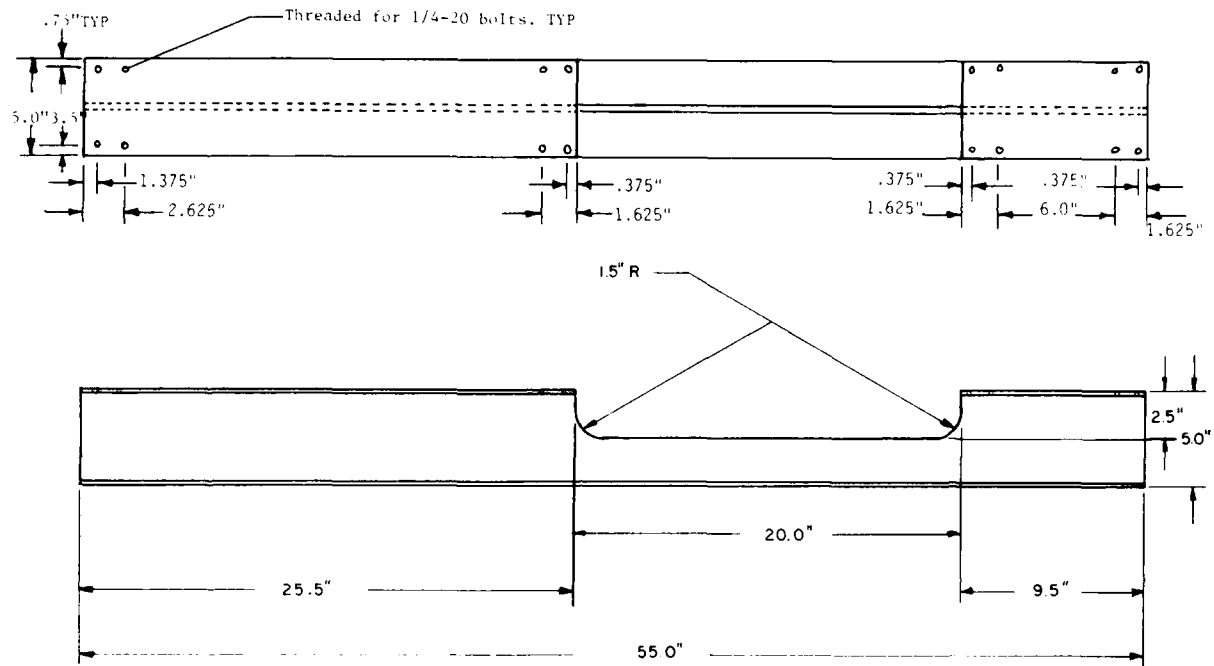


Fig. C33 — Assembly of collimator



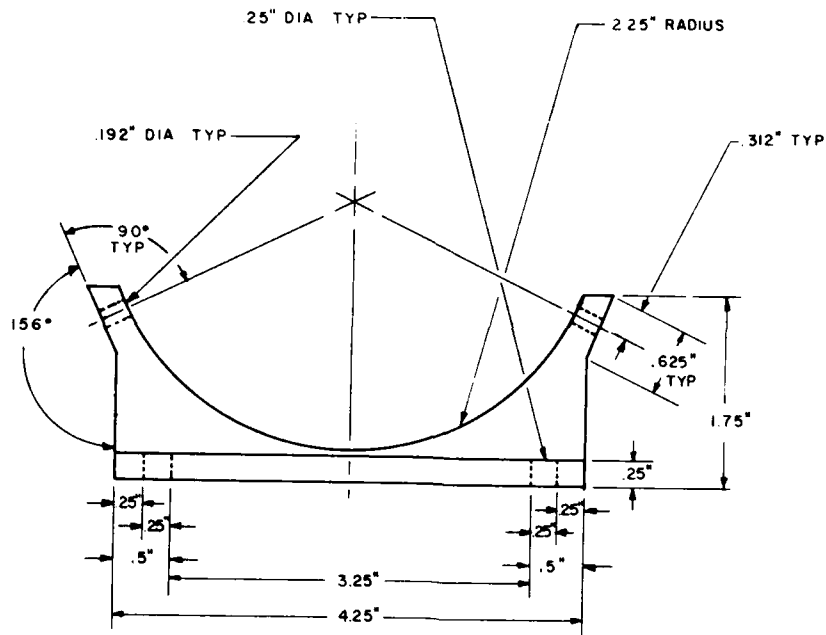
MATERIAL: 6061 T6 ALUMINUM 5" x 5" x .313" WEB H-BEAM

(a)

1. Cut to specified dimensions and tolerances 6061 T6 aluminum 5" x 5" x .313 web H-beam.
2. Piece should be free from burrs and sharp edges.
3. Black anodize and paint white after cutting.

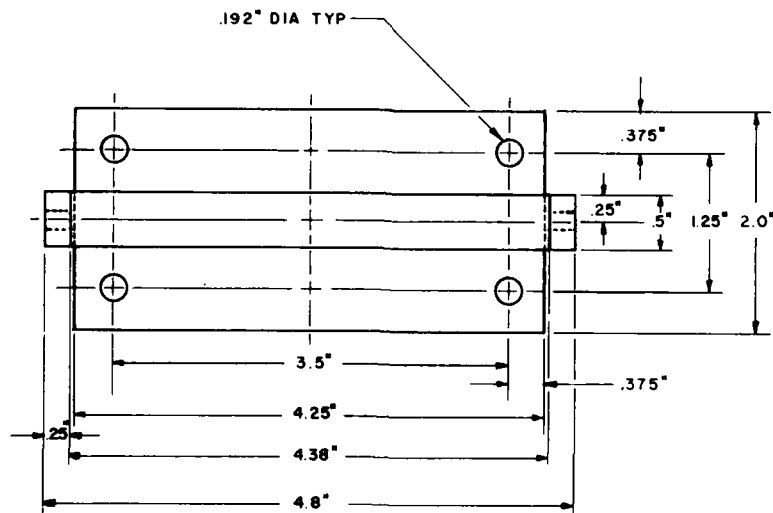
(b)

Fig C34 — FSM sensor base, unless otherwise specified, tolerances are  $\pm .01$   
(a) side and top views and (b) notes



MATERIAL: 6061 T6 ALUMINUM

(a)

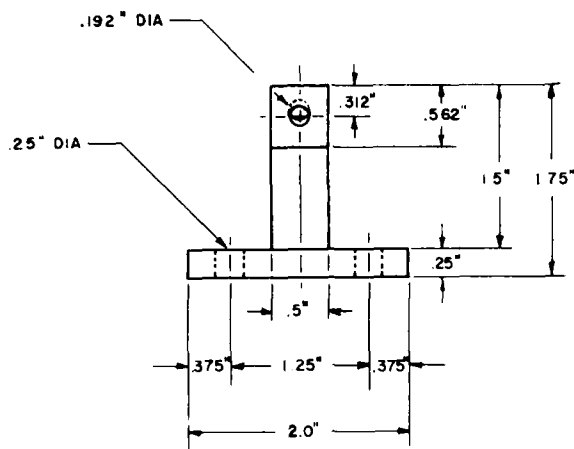


MATERIAL: 6061 T6 ALUMINUM

(b)

Fig. C35 — FSM cradle mounts; unless otherwise specified, tolerances are  $\pm .002$   
 (a) front view, (b) top view, (c) side view and (d) notes

MATERIAL: 6061 T6 ALUMINUM



(c)

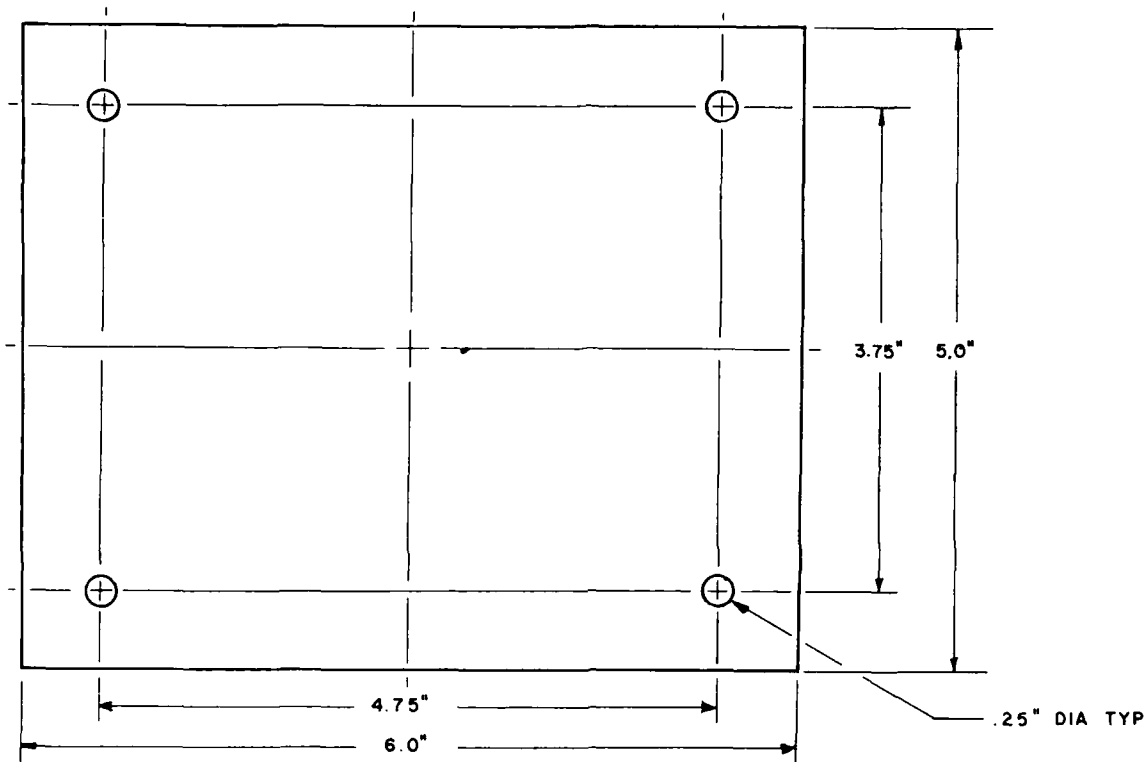
1. Machine to specified dimensions and tolerances from plate aluminum.
2. All dimensions are after finish.
3. Outer diameter of laser and detector tubes must fit in cradle of mount.
4. Black anodize and paint white after machining.
5. Four cradle mounts are needed each of which must be the same height.
6. Piece should be free from all burrs and sharp edges.
7. Piece should have fine finish and good overall appearance.

(d)

Fig. C35 (Continued) — FSM cradle mounts; unless otherwise specified, tolerances are  $\pm .002$   
 (a) front view, (b) top view, (c) side view and (d) notes



MATERIAL: .5" HARD RUBBER



(a)

1. Cut and drill holes to specified dimensions and tolerances.
2. Use 1/2" sheet rubber.
3. Piece should have good overall appearance.

(b)

Fig. C36 — FSM shock mount: (a) top view and (b) notes

(a)

MATERIAL: 6061 T6 ALUMINUM

25" DIA. TYP

1.25"

2.0"

2.0"

4.75"

6.0"

1.5"

2.5" TYP

3.75"

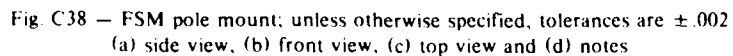
5.0"

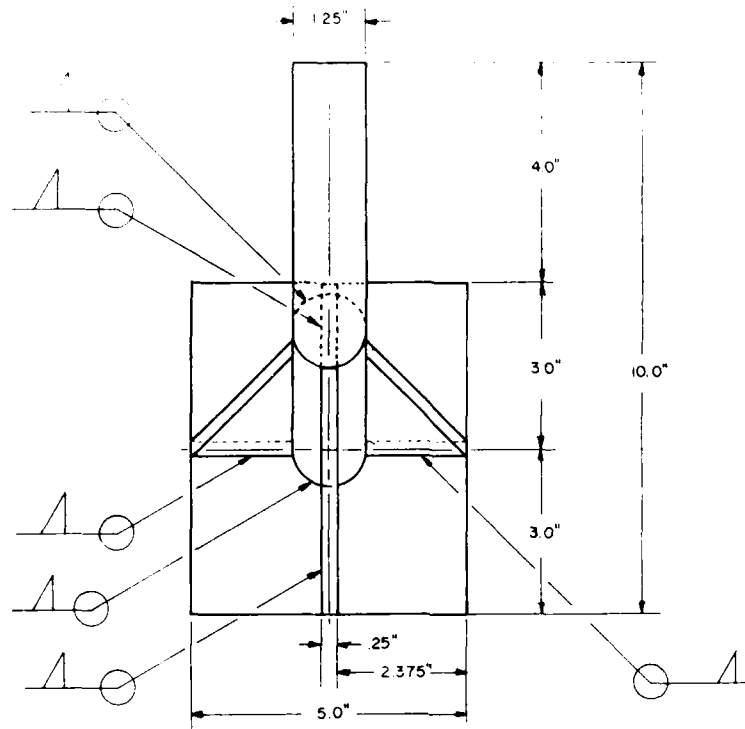
TYP

(b)

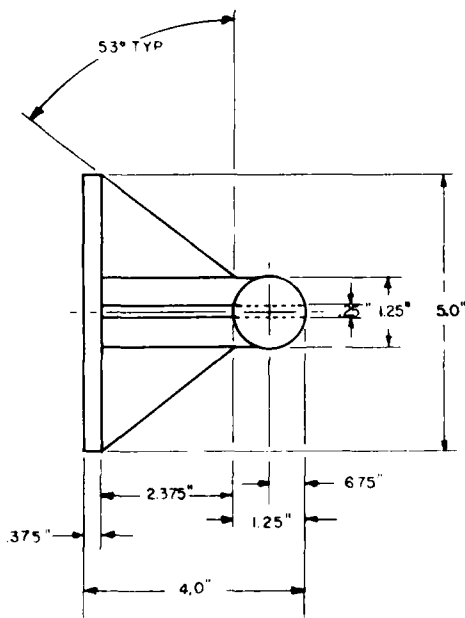
61

Fig. C37 (Continued) — FSM mounting plate; unless otherwise specified, tolerances are  $\pm .002$   
(a) side view, (b) top view and (c) notes





(b)



(c)

1. Cut shafting from 1-1/4" aluminum bar stock.
2. Cut strengthening fins from 1/4" plate aluminum.
3. Cut mounting plate from 3/8" aluminum plate stock.
4. Silver solder all seams.
5. Piece should be free from all burrs and sharp edges.
6. Piece should have smooth finish and have overall good appearance.
7. All dimensions are after finish.
8. Black anodize and paint white after machining.

(d)

Fig. C38 (Continued) — FSM pole mount; unless otherwise specified, tolerances are  $\pm .002$   
(a) side view, (b) front view, (c) top view and (d) notes

64

1. Cut and form from 1/16" sheet aluminum.
2. Continuous weld all seams.
3. Black anodize.

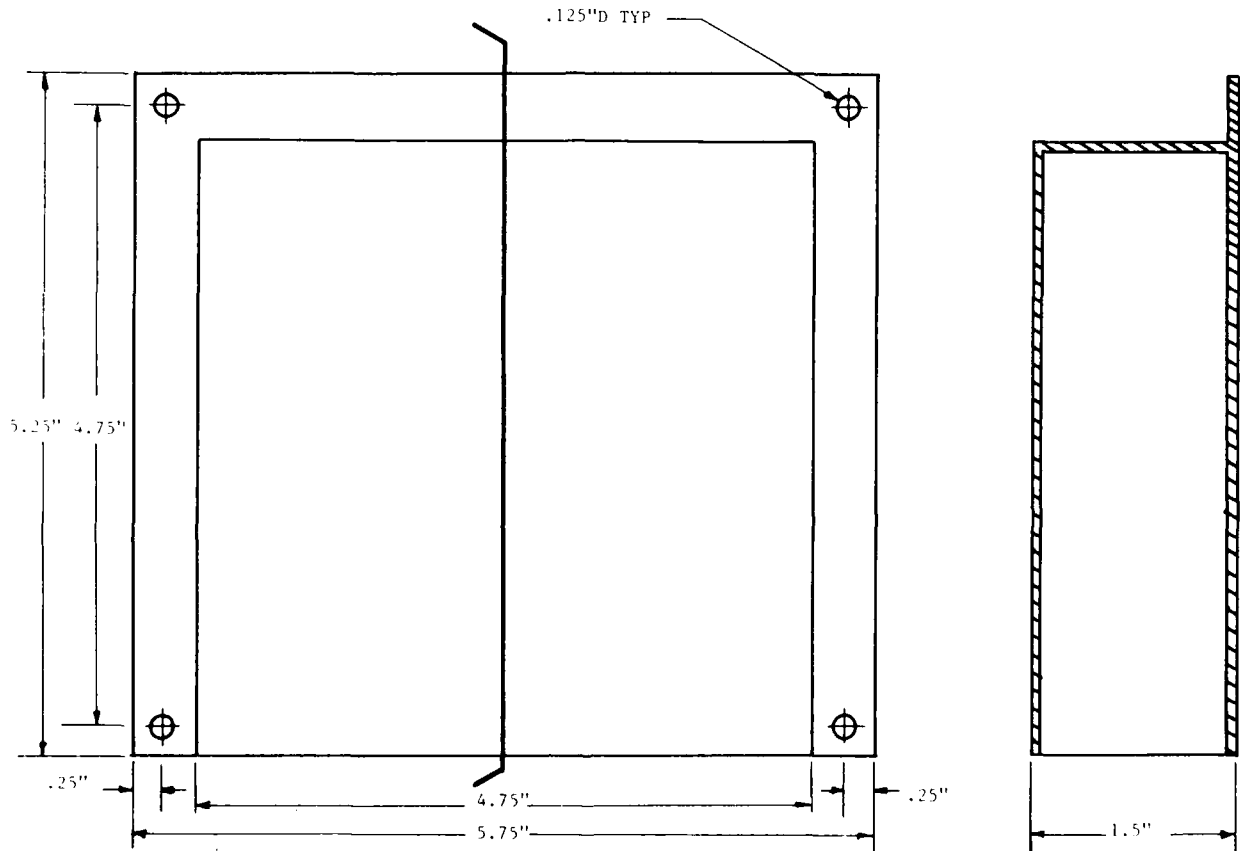


Fig. C40 — Fan cover, front and side sectional views; unless otherwise specified, tolerances are  $\pm .02$

END

2-87

DTIC